

Faculty of MECHANICAL ENGINEERING

Department of TECHNICAL THERMODYNAMICS

# Property Library for R134a

FluidLAB with LibR134a for MATLAB®

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# Property Library for the Calculation of R134a

# FluidLAB for MATLAB® LibR134a

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## 0. Package Contents

#### 0.1 Zip file for 32-bit MATLAB®

The following zip file is delivered for your computer running a 32-bit version of MATLAB®.

#### "CD\_FluidLAB\_LibR134a.zip"

Including the following files:

FluidLAB\_LibR134a\_Setup.exe - Installation program for the FluidLAB Add-On

for use in MATLAB®

LibR134a.dll - Dynamic Link Library for R134a for use

in MATLAB®

FluidLAB\_LibR134a\_Docu\_Eng.pdf - User's Guide

## 0.2 Zip file for 64-bit MATLAB®

The following zip file is delivered for your computer running a 64-bit version of MATLAB®.

#### "CD\_FluidLAB\_LibR134a\_x64.zip"

Including the following files and folders:

#### Files:

Setup.exe - Self-extracting and self-installing program

for FluidLAB

FluidLAB\_LibR134a\_64\_Setup.msi - Installation program for the FluidLAB Add-On

for use in MATLAB®

LibR134a.dll - Dynamic Link Library for R134a for use

in MATLAB®

FluidLAB\_LibR134a\_Docu\_Eng.pdf - User's Guide

#### Folders:

vcredist\_x64 - Folder containing the "Microsoft Visual C++

2010 x64 Redistributable Pack"

WindowsInstaller3\_1 - Folder containing the "Microsoft Windows

Installer"

# 1. Property Functions

Functional Dependence	Function Name	Call from Fortran program	Call in DLL LibR134a as parameter	Property or Function	Unit of the result
a = f(p, t, x)	a_ptx_R134a	A_PTX_R134A(P,T,X)	C_A_PTX_R134A(A,P,T,X)	Thermal diffusivity	m <sup>2</sup> /s
$c_p = f(p, t, x)$	cp_ptx_R134a	CP_PTX_R134A(P,T,X)	C_CP_PTX_R134A(CP,P,T,X)	Specific isobaric heat capacity	kJ/(kg K)
$c_V = f(p, t, x)$	cv_ptx_R134a	CV_PTX_R134A(P,T,X)	C_CV_PTX_R134A(CV,P,T,X)	Specific isochoric heat capacity	kJ/(kg K)
$\eta = f(p, t, x)$	eta_ptx_R134a	ETA_PTX_R134A(P,T,X)	C_ETA_PTX_R134A(ETA,P,T,X)	Dynamic viscosity	Pa s
h = f(p, t, x)	h_ptx_R134a	H_PTX_R134A(P,T,X)	C_H_PTX_R134A(H,P,T,X)	Specific enthalpy	kJ/kg
$\kappa = f(p, t, x)$	kappa_ptx_R134a	KAP_PTX_R134A(P,T,X)	C_KAP_PTX_R134A(KAP,P,T,X)	Isentropic exponent	-
$\lambda = f(p, t, x)$	lambda_ptx_R134a	LAM_PTX_R134A(P,T,X)	C_LAM_PTX_R134A(LAM,P,T,X)	Thermal conductivity	W/m K
V = f(p, t, x)	ny_ptx_R134a	NY_PTX_R134A(P,T,X)	C_NY_PTX_R134A(NY,P,T,X)	Kinematic viscosity	m <sup>2</sup> /s
$p_{s} = f(t)$	ps_t_R134a	PS_T_R134A(T)	C_PS_T_R134A(PS,T)	Vapor pressure from temperature	Bar
Pr = f(p, t, x)	Pr_ptx_R134a	PR_PTX_R134A(P,T,X)	C_PR_PTX_R134A(PR,P,T,X)	Prandtl-Number	-
$\rho = f(p, t, x)$	rho_ptx_R134a	RHO_PTX_R134A(P,T,X)	C_RHO_PTX_R134A(RHO,P,T,X)	Density	kg/m³
s = f(p, t, x)	s_ptx_R134a	S_PTX_R134A(P,T,X)	C_S_PTX_R134A(S,P,T,X)	Specific entropy	kJ/(kg K)
$\sigma = f(t)$	sigma_t_R134a	SIGMA_T_R134A(T)	C_SIGMA_T_R134A(SIGMA,T)	Surface tension	N/m
t = f(p,h)	t_ph_R134a	T_PH_R134A(P,H)	C_T_PH_R134A(T,P,H)	Backward function: Temperature from pressure and enthalpy	°C
t = f(p,s)	t_ps_R134a	T_PS_R134A(P,S)	C_T_PS_R134A(T,P,S)	Backward function: Temperature from pressure and entropy	°C
$t_{\rm S} = {\sf f}(p)$	ts_p_R134a	TS_P_R134A(P)	C_TS_P_R134A(TS,P)	Saturation temperature from pressure	°C
u = f(p, t, x)	u_ptx_R134a	U_PTX_R134A(P,T,X)	C_U_PTX_R134A(U,P,T,X)	Specific internal energy	kJ/kg
V = f(p, t, x)	v_ptx_R134a	V_PTX_R134A(P,T,X)	C_V_PTX_R134A(V,P,T,X)	Specific volume	m³/kg
W = f(p, t, x)	w_ptx_R134a	W_PTX_R134A(P,T,X)	C_W_PTX_R134A(W,P,T,X)	Isentropic speed of sound	m/s²
x = f(p,h)	x_ph_R134a	X_PH_R134A(P,H)	C_X_PH_R134A(X,P,H)	Backward function: Vapor fraction from pressure and enthalpy	kg/kg
x = f(p,s)	x_ps_R134a	X_PS_R134A(P,S)	C_X_PS_R134A(X,P,S)	Backward function: Vapor fraction from pressure and entropy	kg/kg

**Units:** t in °C

p in bar

x in (kg of saturated steam)/(kg wet steam)

#### Range of validity

Temperature range: from  $t(p, \rho_{max})$  to 181.85 °C

Pressure range: from  $p_t = 0.000389564$  bar to 700 bar

#### Reference state

h = 200 kJ/kg and s = 1 kJ/(kg K) at  $t = 0 ^{\circ}\text{C}$  on the saturated liquid line (x = 0)

#### Details on the vapor fraction x

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

#### Single-phase region

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

#### Wet-steam region

If the state point to be calculated is located in the wet steam region, a value for x between 0 and 1 (x = 0 for saturated liquid, x = 1 for saturated steam) must be entered. In this case, the backward functions result in the appropriate value between 0 and 1 for x. When calculating wet steam either the given value for t and t = -1000 or the given value for t and t = -1000 and in both cases the value for t between 0 and 1 must be entered.

If p and t and x are entered as given values, the program considers p and t to be appropriate to represent the vapor pressure curve. If this is not the case the calculation for the property of the chosen function results in -1000.

Wet steam region: Temperature ranges from  $t_{\rm t} = -103.30~{\rm ^{\circ}C}$  to  $t_{\rm c} = 101.03~{\rm ^{\circ}C}$ 

Pressure ranges from  $p_t = 0.000389564$  bar to  $p_c = 40.566$  bar

#### Hint:

If the calculation results in –1000, the values entered represent a state point beyond the range of validity of LibR134a. For further information on each function and its range of validity see Chapter 3. The same information may also be accessed via the online help pages.

# 2 Application of FluidLAB in MATLAB®

The FluidLAB Add-In has been developed to calculate thermodynamic properties in MATLAB® more conveniently. Within MATLAB® it enables the direct call of functions relating to R134a from the LibR134a property library.

#### 2.1 Installing FluidLAB

#### Installing FluidLAB including LibR134a for 32-bit MATLAB®

This section describes the installation of FluidLAB LibR134a for a 32-bit version of MATLAB<sup>®</sup>. Before you begin, it is best to close any Windows<sup>®</sup> applications, since Windows<sup>®</sup> may need to be rebooted during the installation process.

After you have downloaded and extracted the zip-file "CD\_FluidLAB\_LibR134a.zip", you will see the folder

CD\_FluidLAB\_LibR134a

in your Windows Explorer®, Norton Commander® or another similar program you are using.

Open this folder by double-clicking on it.

In this folder you will see the following files:

FluidLAB\_LibR134a\_Docu\_Eng.pdf FluidLAB\_LibR134a\_Setup.exe LibR134a.dll.

In order to run the installation of FluidLAB including, the LibR134a property library, double-click on the file

FluidLAB\_LibR134a\_Setup.exe.

Installation may start with a window noting that all Windows® programs should be closed. When this is the case, the installation can be continued. Click the "Next >" button.

In the following dialog box, "Destination Location", the default path offered automatically for the installation of FluidLAB is

C:\Program Files\FluidLAB\LibR134a (for English version of Windows)
C:\Programme\FluidLAB\LibR134a (for German version of Windows).

By clicking the "Browse..." button, you can change the installation directory before installation (see Figure 2.1).



Figure 2.1: "Destination Location"

If you wish to change directories, click the "Browse..." button and select your desired directory. The instructions in this documentation refer to the stated default directory. Leave this window by clicking the "Next >" button.

The dialog window "Start Installation" pops up. Click the "Next >" button to continue installation. The FluidLAB files are now being copied into the created directory on your hard drive. Click the "Finish >" button in the following window to complete installation.

The installation program has copied the following files for LibR134a into the directory:

C:\Program Files\FluidLAB\LibR134a (for English version of Windows)
C:\Programme\FluidLAB\LibR134a (for German version of Windows)):

advapi32.dll LC.dll

Dformd.dll msvcp60.dll
Dforrt.dll msvcrt.dll
INSTALL.LOG Unwise.exe
LibR134a.dll Unwise.ini

Now, you have to overwrite the file "LibR134a.dll" in your FluidLAB directory with the file of the same name provided on your CD with FluidLAB.

To do this, open the CD in "My Computer" and click on the file "LibR134a.dll" in order to highlight it. Then click on the "Edit" menu in your Explorer and select "Copy".

Now, open your FluidLAB directory (the standard being

C:\Program Files\FluidLAB\LibR134a (for English version of Windows)
C:\Programme\FluidLAB\LibR134a (for German version of Windows))

and insert the file "LibR134a.dll" by clicking the "Edit" menu in your Explorer and then select "Paste". Answer the question whether you want to replace the file by clicking the "Yes" button. Now, you have overwritten the file "LibR134a.dll" successfully and the property functions are available in MATLAB.

## Installing FluidLAB including LibR134a for 64-bit MATLAB®

This section describes the installation of FluidLAB LibR134a.

Before you begin, it is best to close any Windows® applications, since Windows® may need to be rebooted during the installation process.

After you have downloaded and extracted the zip-file "CD\_FluidLAB\_LibR134a\_x64.zip", you will see the folder

CD FluidLAB LibR134a

in your Windows Explorer®, Norton Commander® or any other similar program you are using.

Open this folder by double-clicking on it.

In this folder you will see the following files

FluidLAB\_LibR134a\_Docu\_Eng.pdf FluidLAB\_LibR134a\_64\_Setup.msi

LibR134a.dll

Setup.exe

and folders

/vcredist\_x64

/WindowsInstaller3 1.

In order to run the installation of FluidLAB including, the LibR134a property library, double-click on the file

Setup.exe.

Installation of FluidLAB LibR134a starts with a window noting that the installer will guide you through the installation process. Click the "Next >" button to continue.

In the following dialog box, "Destination Location", the default path offered automatically for the installation of FluidLAB is

C:\Program Files\FluidLAB\LibR134a (for English version of Windows)
C:\Programme\FluidLAB\LibR134a (for German version of Windows)

By clicking the "Browse..." button, you can change the installation directory before installation (see Figure 2.2).



Figure 2.2: "Select Installation Folder"

Finally, click on "Next >" to continue installation; click "Next >" again in the "Confirm Installation" window which follows in order to start the installation of FluidLAB.

After FluidLAB has been installed, you will see the sentence "FluidLAB LibR134a 64 has been successfully installed." Confirm this by clicking the "Close" button.

The installation program has copied the following files for LibR134a into the directory

"C:\Program Files\FluidLAB\LibR134a" (for English version of Windows)
"C:\Programme\FluidLAB\LibR134a" (for German version of Windows):

capt\_ico\_big.ico libifcoremd.dll
LC.dll libiomp5md.dll
LibR134a.dll libmmd.dll

Now, you have to overwrite the file "LibR134a.dll" in your FluidLAB directory with the file of the same name provided on your CD with FluidLAB.

To do this, open the CD in "My Computer" and click on the file "LibR134a.dll" in order to highlight it. Then click on the "Edit" menu in your Explorer and select "Copy".

Now, open your FluidLAB directory (the standard being

"C:\Program Files\FluidLAB\LibR134a" (for English version of Windows)
"C:\Programme\FluidLAB\LibR134a" (for German version of Windows))

and insert the file "LibR134a.dll" by clicking the "Edit" menu in your Explorer and then select "Paste". Answer the question whether you want to replace the file by clicking the "Yes" button. Now, you have overwritten the file "LibR134a.dll" successfully and the property functions are available in MATLAB.

The installation programs for both the 32-bit and the 64-bit Windows version have copied the following function files for LibR134a into the directory

"C:\Program Files\FluidLAB\LibR134a" (for English version of Windows)
"C:\Programme\FluidLAB\LibR134a" (for German version of Windows):

- Dynamic Link Library "LibR134a.dll" and other necessary system DLL files.
- MATLAB®-Interface-Program for calculable functions

a\_ptx\_R134a rho\_ptx\_R134a cp\_ptx\_R134a s\_ptx\_R134a cv\_ptx\_R134a t\_ph\_R134a eta ptx R134a t ps R134a h\_ptx\_R134a ts\_p\_R134a kappa\_ptx\_R134a u\_ptx\_R134a lambda\_ptx\_R134a v\_ptx\_R134a ny\_ptx\_R134a w\_ptx\_R134a Pr\_ptx\_R134a x\_ph\_R134a ps\_t\_R134a x\_ps\_R134a

Please note that there is a difference in the file extension of the function files.

The 32-bit installation program has copied function files with the file extension

.mexw32

and the 64-bit installation program has copied function files with the file extension

.mexw64

into your LibR134a directory (the standard being

"C:\Program Files\FluidLAB\LibR134a" (for English version of Windows)
"C:\Programme\FluidLAB\LibR134a" (for German version of Windows)).

#### 2.2 Licensing the LibR134a Property Library

The licensing procedure must be carried out when the prompt message appears. In this case, you will see the "License Information" window for LibR134a (see figure below).



Figure 2.3: "License Information" window

Here you are asked to type in the license key which you have obtained from the Zittau/Goerlitz University of Applied Sciences. If you do not have this, or have any questions, you will find contact information on the "Content" page of this User's Guide or by clicking the yellow question mark in the "License Information" window. Then the following window will appear:



Figure 2.4: "Help" window

If you do not enter a valid license it is still possible to use MATLAB® by clicking "Cancel". In this case, the LibR134a property library will display the result "–11111111" for every calculation.

The "License Information" window will appear every time you use FluidLAB LibR134a until you enter a license code to complete registration. If you decide not to use FluidLAB LibR134a, you can uninstall the program following the instructions given in section 2.5 of this User's Guide.

#### 2.3 Example: Calculation of h = f(p,t,x) in an M-File

Now we will calculate, step by step, the specific enthalpy h as a function of pressure p, temperature t and vapor fraction x using FluidLAB.

Please carry out the following instructions:

- Start Windows Explorer<sup>®</sup>, Total Commander<sup>®</sup>, My Computer or another file manager program. The following description refers to Windows Explorer<sup>®</sup>.
- Your Windows Explorer<sup>®</sup> should be set to "Details" for easier viewing. Click the "Views" button and select "Details."
- Switch into the program directory of FluidLAB, in which you will find the folder "\LibR134a"; it is generally saved under: "C:\Program Files\FluidLAB"
- Create the folder "\LibR134a\_Example" by clicking on "File" in the Explorer<sup>®</sup> menu, then "New" in the menu which appears and afterwards selecting "Folder". Name the new folder "\LibR134a Example."
- You will now see the following window:

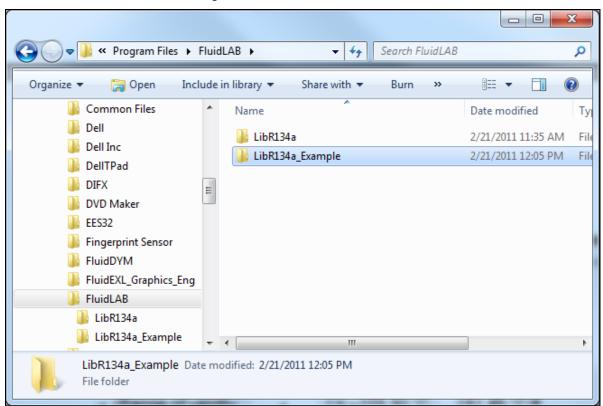


Figure 2.5: Folders "LibR134a" and "LibR134a\_Example"

- Switch into the directory "\LibR134a" within "\FluidLAB", the standard being
- "C:\Program Files\FluidLAB\LibR134a"

(for English version of Windows)

"C:\Programme\FluidLAB\LibR134a"

(for German version of Windows))."

- You will see the following window:

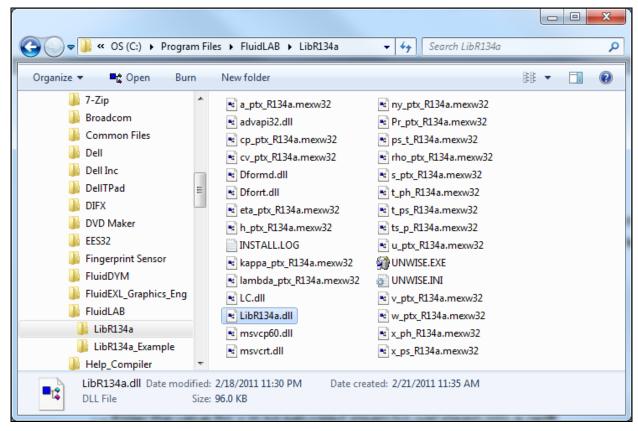


Figure 2.6: Contents of the folder "LibR134a"

If you have installed the <u>32-bit version</u> of LibR134a you will now have to copy the following files into the directory

- "C:\Program Files\FluidLAB\LibR134a\_Example" (for English version of Windows)
- "C:\Programme\FluidLAB\LibR134a\_Example" (for German version of Windows)

in order to calculate the function h = f(p,t,x).

- The following files are needed:
  - "h\_ptx\_97.mexw32"
  - "LibR134a.dll"
  - "libifcoremdd.dll"
  - "libmmd.dll"
  - "libmmdd.dll"
  - "msvcr71d.dll"
  - "dforrt.dll.dll"
  - "msvcrt.dll"
- Click the file "h\_ptx\_R134a.mexw32", then click "Edit" in the upper menu bar and select "Copy".
- Switch into the directory
  - "C:\Program Files\FluidLAB\LibR134a\_Example" (for English version of Windows)
  - "C:\Programme\FluidLAB\LibR134a\_Example" (for German version of Windows),

click "Edit" and select "Paste".

- Repeat these steps in order to copy the other files listed above.

You may also select all the above-named files and then copy them as a group (press the Control button to enable multiple markings).

- You will see the following window:

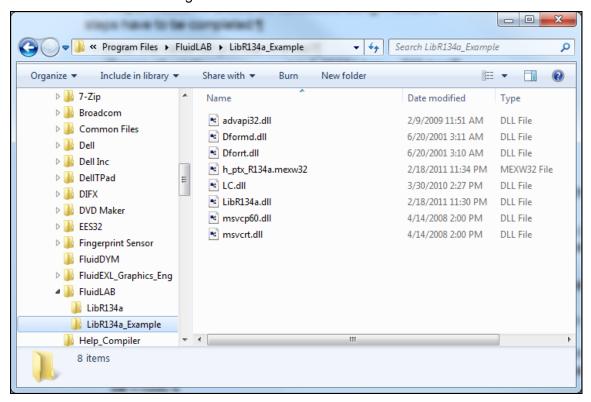


Figure 2.7: Contents of the folder "LibR134a\_Example"

If you have installed the <u>64-bit version</u> of LibR134a you will now have to copy the following files into the directory

"C:\Program Files\FluidLAB\LibR134a\_Example" (for English version of Windows)

"C:\Programme\FluidLAB\LibR134a\_Example" (for German version of Windows)

in order to calculate the function h = f(p,t,x).

- The following six files are needed:
  - "h\_ptx\_R134a.mexw64"
  - "LC.dll"
  - "LibR134a.dll"
  - "libifcoremd.dll"
  - "libiomp5.dll"
  - "libmmd.dll."
- Click the file "h\_ptx\_R134a.mexw64", then click "Edit" in the upper menu bar and select "Copy."
- Switch into the directory

"C:\Program Files\FluidLAB\LibR134a\_Example" (for English version of Windows) "C:\Programme\FluidLAB\LibR134a\_Example" (for German version of Windows),

click "Edit" and then "Paste."

- Repeat these steps in order to copy the other files listed above. You may also select all the above-named files and then copy them as a group (press the Control button to enable multiple markings).
- Now, start MATLAB (if you have not started it before).
- Click the button marked in the next figure in order to open the folder "\LibR134a\_Example" in the "Current Folder" window.

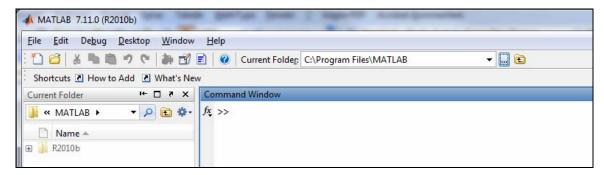


Figure 2.8: Selection of the working directory

- Find and select the directory "C:\Program Files\FluidLAB\LibR134a\_Example" in the pop-up menu (see the following figure).

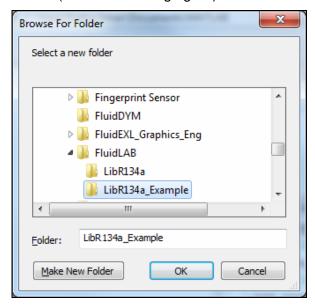


Figure 2.9: Choosing the "LibR134a\_Example" folder

- Confirm your selection by clicking the "OK" button.
- First of all you need to create an M–File in MATLAB<sup>®</sup>. Within MATLAB<sup>®</sup> click "Desktop", then select "Editor". Now click on the "New Script" button in the Editor Window.
- If the "Editor" window appears as a separate window, you can embed it into MATLAB<sup>®</sup> by clicking the insertion arrow (see next figure) in order to obtain a better view.

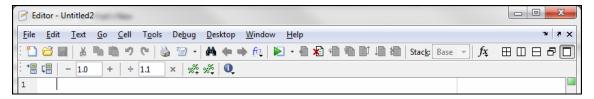


Figure 2.10: Embedding the "Editor" window

- In the following figure you will see the "Editor – Untitled" window.

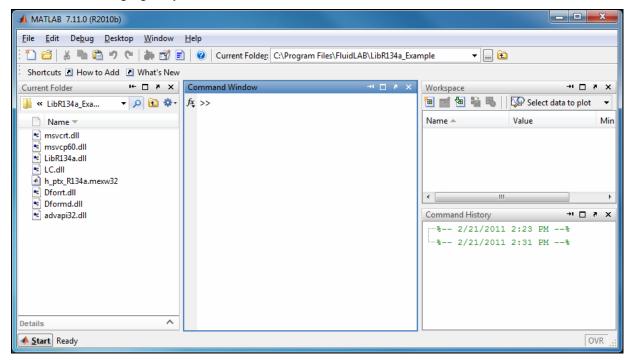


Figure 2.11: Embedded "Editor" window

Now type the following lines in the "Editor - Untitled" window:

Text to be written:	Explanation:	
% h_ptx_R134a.m	file name as comment	
	paragraph separation	
p=10; % pressure in bar	declaration of the	
t=25; % temperature in °C	variables pressure,	
x=-1; % vapor fraction in kg/kg	temperature, art and composition of mixture	
%%	paragraph separation	
h=h_ptx_R134a(p,t,x)	function call	
%%	paragraph separation	

#### - Remarks:

- The program interprets the first line, starting with "%," to be a data description in "Current Directory."
- Paragraph separations which are mandatory are marked with "%%". This also serves to separate the declaration of variables and calculation instructions.

- The words which are printed in green, start with "%" and come after the variables are comments. They are not in fact absolutely necessary, but they are very helpful for your overview and to make the process more easily understood.
- Omit the semicolons after the numerical values if you wish to see the result for *h* and the input parameters.

The values of the function parameters in their corresponding units stand for:

```
- First operand: Value for p = 10 (Range of validity: p = 0.00391 bar ... 700 bar)
```

- Second operand: Value for t = 25 °C (Range of validity: t = -103.30 °C ... 181.85 °C)

- Third operand: Value for x = -1 kg/kg

Since the wet steam region is calculated automatically by the subprograms, the following fixed details on the vapor fraction *x* are to be considered when the value for x is entered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam), e. g., pressure p and temperature t are given, x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located in the wet steam region, a value for x between 0 and 1 (x = 0 for saturated liquid, x = 1 for saturated steam) must be entered.

When calculating wet steam either the given value for t and p = -1000 or the given value for p and t = -1000, plus the value for x between 0 and 1 must be entered.

If p and t and x are entered as given values, the program considers p and t to be appropriate to represent the vapor pressure curve. If this is not the case the enthalpy calculated later will result in -1000.

```
(Vapor pressure curve of R134a: t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3) \dots t_{\text{C}} = 101.03 \text{ °C}

p_{\text{t}} = 0.00389564 \text{ bar} \dots p_{\text{C}} = 40.566 \text{ bar})
```

- Save the "M-File" by clicking the "File" button and then click "Save As...".
- The menu "Save file as:" appears; In this menu, the folder name "LibR134a\_Example" must be displayed in the "Save in:" field.
- Next to "File name" you have to type "Example\_h\_ptx\_R134a.m" and afterwards click the "Save" button.

#### Note.

The name of the example file has to be different in comparison to the name of the used function. For example, the file could not be named "h\_ptx\_R134a.m" in this case. Otherwise an error message will appear during the calculation.

- You will now see the following window:

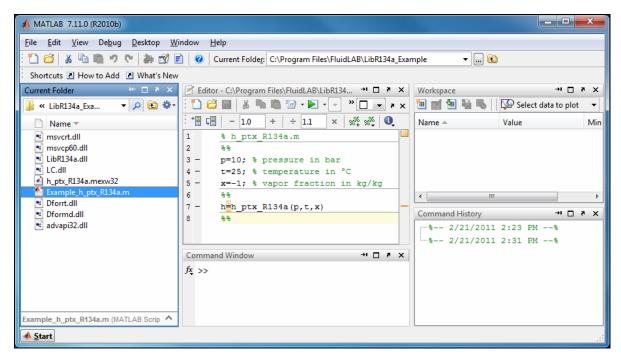


Figure 2.12: "Example\_h\_ptx\_R134a.m" M-file

- Within the "Current Folder" window, the file "Example\_h\_ptx\_R134a.m" appears.
- Right-click on this file and select "Run" in the menu which appears (see next figure).

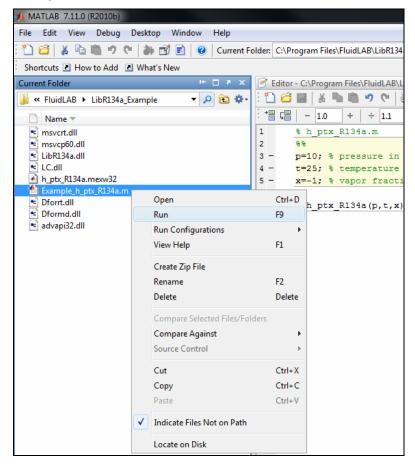


Figure 2.13: Running the "Example\_h\_ptx\_R134a.m" M-file

You will see the following window:

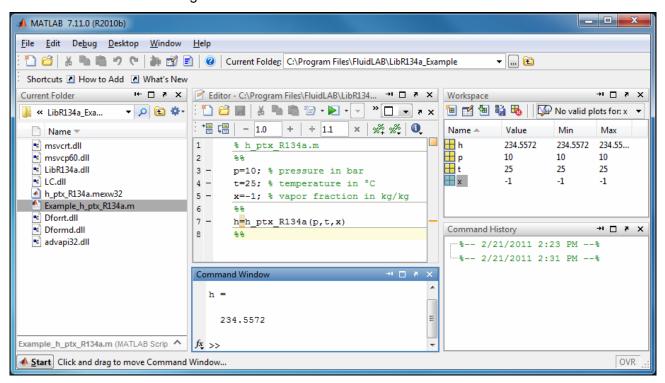


Figure 2.14: MATLAB® with calculated result

The result for *h* appears in the "Command Window".

 $\Rightarrow$  The result in our sample calculation here is: "h = 234.5572". The corresponding unit is kJ/kg (see table of the property functions in Chapter 1).

To be able to calculate other values, you have to copy the associated mexw32 files as well because MATLAB® can only access functions that are located in the "Current Directory" window. The example calculated can be found in the directory

C:\Program Files\FluidLAB\LibR134a\_Example," and you may use it as a basis for further calculations using FluidLAB.

#### 2.4 Example: Calculation of h = f(p,t,x) in the Command Window

- Start MATLAB® (if you have not started it already).
- Click the button marked in the following image in order to open the folder "\LibR134a\_Example" in the window "Current Folder."

(for English version of Windows)

(for German version of Windows)

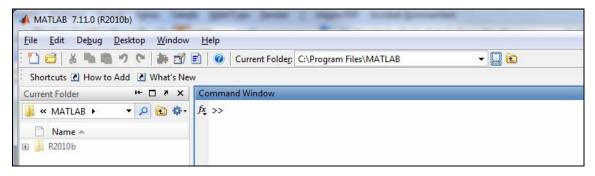


Figure 2.15: Selection of the working directory

- Find and select the directory

"C:\Program Files\FluidLAB\LibR134a\_Example"

"C:\Programme\FluidLAB\LibR134a\_Example"

in the menu which appears (see the following figure).

Figure 2.16: Choosing the "LibR134a\_Example" folder

- Confirm your selection by clicking the "OK" button.
- You will see the following window:

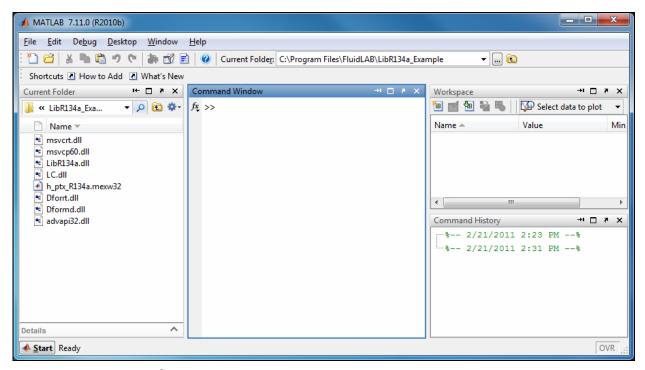


Figure 2.17: MATLAB® with necessary files

Corresponding to the table of the property functions in Chapter 1 you have to call up the function  $"h_ptx_R134a"$  as follows for calculating h = f(p,t,x).

Write "h=h\_ptx\_R134a(10,25,-1)" within the "Command Window"

The values of the function parameters in their corresponding units stand for:

```
    First operand: Value for p = 10 bar (Range of validity: p = 0.00391 bar ... 700 bar)
    Second operand: Value for t = 25 °C (Range of validity: t = -103.30 °C ... 181.85 °C)
```

- Third operand: Value for x = -1

Since the wet steam region is calculated automatically by the subprograms, the following fixed details on the vapor fraction *x* are to be considered when the value for *x* is entered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam), e. g., pressure p and temperature t are given, x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located in the wet steam region, a value for x between 0 and 1 (x = 0 for saturated liquid, x = 1 for saturated steam) must be entered.

When calculating wet steam either the given value for t and p = -1000 or the given value for p and t = -1000, plus the value for x between 0 and 1 must be entered.

If p and t and x are entered as given values, the program considers p and t to be appropriate to represent the vapor pressure curve. If this is not the case the enthalpy calculated later will result in -1000.

```
(Vapor pressure curve of R134a: t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3) \dots t_{\text{C}} = 101.03 \text{ °C}

p_{\text{t}} = 0.00389564 \text{ bar} \dots p_{\text{C}} = 40.566 \text{ bar})
```

- Confirm your entry by pressing the "ENTER" button.
- You will see the following window:

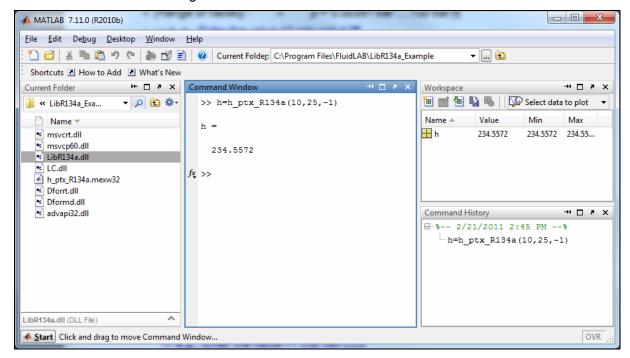


Figure 2.18: MATLAB® with calculated result

 $\Rightarrow$  In the "Command Window" you will see the result "h = 234.5572". The corresponding unit is kJ/kg (see table of the property functions in Chapter 1).

To be able to calculate other values, you will have to copy the respective mexw32 or mexw64 files into the working directory as well because MATLAB® can only access functions that are located in the "Current Directory" window.

#### 2.5 Removing FluidLAB including LibR134a

To remove the property library LibR134a from your hard disk drive in Windows<sup>®</sup>, click "Start" in the Windows<sup>®</sup> task bar, select "Settings" and click "Control Panel".

Now double-click on "Add or Remove Programs". In the list box of the "Add or Remove Programs" window that appears select "FluidLAB LibR134a" by clicking on it and click the "Change/Remove" button.

In the following dialog box click "Automatic" and then click the "Next >" button.

Confirm the following menu "Perform Uninstall" by clicking the "Finish" button.

Finally, close the "Add or Remove Programs" and "Control Panel" windows. Now, FluidLAB has been removed.

If there is no library other than LibR134a installed, the directory "FluidLAB" will be removed as well.

# 3. Program Documentation

# Thermal Diffusivity a = f(p,t,x)

Function Name: a\_ptx\_R134a

Subroutine with function value: REAL\*8 FUNCTION A\_PTX\_R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_A\_PTX\_R134A(A,P,T,X)

for call from DLL: REAL\*8 A,P,T,X

#### **Input Values:**

**P** - Pressure *p* in bar

T - Temperature t in °C

**X** - Vapor fraction *x* (kg of saturated steam)/(kg wet steam)

#### Result

**A\_PTX\_R134A**, **A** or **a\_ptx\_R134a** – Thermal diffusivity 
$$a = \frac{\lambda * v}{c_p}$$
 in m<sup>2</sup>/s

#### Range of validity

Temperature range: from - 73.15 °C to 176.85 °C

Pressure range: from 0.00389564 bar to 700 bar

Density range: from  $0.00105455 \text{ kg/m}^3$  to  $1550 \text{ kg/m}^3$ 

# Details on the vapor fraction *x* and on the calculation of saturated liquid and saturated steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located on the saturated liquid line, x = 0 must be entered. When calculating saturated steam (saturated vapor line) x = 1 must be entered.

The calculation for x-values between 0 and 1 is not possible.

When calculating saturated liquid or saturated steam, it is adequate to enter either the given value for t and p = -1000, or the given value for p and t = -1000, plus the value for x (x = 0 or x = 1). If p and t and t are entered as given values, the program will consider p and t to be appropriate to represent the vapor pressure curve.

Saturated liquid and saturated vapor line:

Temperature range from t = -73.15 °C to  $t_c = 101.03$  °C

Pressure range from  $p_t = 0.00389564$  bar to  $p_c = 40.566$  bar

#### Results for wrong input values

Result  $A_PTX_R134A$ , A = -1000 or  $a_ptx_R134a = -1000$  for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or t < -103.3°C or  $\rho > 1550$  m<sup>3</sup> / kg

Saturation lines: at p = -1000 and t > 101.03 °C or t < 73.15°C

at t = -1000 and p > 40.566 bar or p < 0.00389564bar or

at p > 40.566 bar or p < 0.00389564 bar and

*t* > 101.03 °C or *t* < -103.3 °C

**References:** [16], [23]

# Specific Isobaric Heat Capacity $c_p = f(p, t, x)$

Function Name: cp\_ptx\_R134a

Subroutine with function value: REAL\*8 FUNCTION CP\_PTX\_R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_CP\_PTX\_R134A(CP,P,T,X)

for call from DLL: REAL\*8 CP,P,T,X

#### **Input Values:**

**P** - Pressure *p* in bar

T - Temperature t in °C

**X** - Vapor fraction *x* (kg of saturated steam)/(kg wet steam)

#### Result

**CP\_PTX\_R134A**, **CP** or **cp\_ptx\_R134a** – Specific isobaric heat capacity  $c_p$  in kJ/(kg K)

#### Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

# Details on the vapor fraction x and on the calculation of saturated liquid and saturated steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located on the saturated liquid line, x = 0 must be entered. When calculating saturated steam (saturated vapor line) x = 1 must be entered.

The calculation for x-values between 0 and 1 is not possible.

When calculating saturated liquid or saturated steam, it is adequate to enter either the given value for t and p = -1000, or the given value for p and t = -1000, plus the value for x (x = 0 or x = 1). If p and t and t are entered as given values, the program will consider t and t to be appropriate to represent the vapor pressure curve. If it is not the case the calculation for the quantity of the chosen function to be calculated results in -1000.

Saturated liquid and saturated vapor line:

Temperature range from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to  $t_{\text{C}} = 101.03 \text{ °C}$ Pressure range from  $p_{\text{t}} = 0.00389564 \text{ bar to } p_{\text{c}} = 40.566 \text{ bar}$ 

#### Results for wrong input values

Result CP\_PTX\_R134A, CP = -1000, or cp\_ptx\_R134a = -1000 for input values:

Single phase region: p > 700 bar or p < 0.00389564bar or

(x = -1) t > 181.85°C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  or  $\rho > 1550 \text{ kg/m}^3$ 

Saturation lines: at p = -1000 and t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ 

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and

t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ 

## Specific Isochoric Heat Capacity $c_v = f(p, t, x)$

Function Name: cv\_ptx\_R134a

Subroutine with function value: REAL\*8 FUNCTION CV\_PTX\_R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_CV\_PTX\_R134A(CV,P,T,X)

for call from DLL: REAL\*8 CV,P,T,X

#### **Input Values:**

**P** - Pressure *p* in bar

T - Temperature t in °C

**X** - Vapor fraction x (kg of saturated steam)/(kg wet steam)

#### Result

CV\_PTX\_R134A, CV or cv\_ptx\_R134a - Specific isochoric heat capacity  $c_v$  in kJ/(kg K)

#### Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

# Details on the vapor fraction x and on the calculation of saturated liquid and saturated steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located on the saturated liquid line, x = 0 must be entered. When calculating saturated steam (saturated vapor line) x = 1 must be entered.

The calculation for *x*-values between 0 and 1 is not possible.

When calculating saturated liquid or saturated steam, it is adequate to enter either the given value for t and p = -1000, or the given value for p and t = -1000, plus the value for x (x = 0 or x = 1). If p and t and t are entered as given values, the program will consider p and t to be appropriate to represent the vapor pressure curve. If it is not the case the calculation for the quantity of the chosen function to be calculated results in -1000.

Saturated liquid and saturated vapor line:

Temperature range from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to  $t_{\text{c}} = 101.03 \text{ °C}$ Pressure range from  $p_{\text{t}} = 0.00389564 \text{ bar to } p_{\text{c}} = 40.566 \text{ bar}$ 

#### Results for wrong input values

Result CV\_PTX\_R134A, CV = -1000 or cv\_ptx\_R134a = -1000 for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  or  $\rho > 1550 \text{ m}^3 / \text{kg}$ 

Saturation lines: at p = -1000 and t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ 

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and

t > 101.03 °C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$ 

## Dynamic Viscosity $\eta = f(p, t, x)$

**Function Name:** eta ptx R134a

**REAL\*8 FUNCTION ETA\_PTX\_R134A(P,T,X)** Subroutine with function value:

for call from Fortran: REAL\*8 P,T,X

INTEGER\*4 FUNCTION C ETA PTX R134A(ETA,P,T,X) Subroutine with parameter:

for call from DLL: REAL\*8 ETA,P,T,X

#### Input Values:

P - Pressure p in bar

T - Temperature t in °C

**X** - Vapor fraction x (kg of saturated steam)/(kg wet steam)

#### Result

ETA PTX R134A, ETA or eta ptx R134a – Dynamic viscosity  $\eta$  in Pa s

#### Range of validity

from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C Temperature range:

from 0.00389564 bar to 700 bar Pressure range:

#### Details on the vapor fraction x and on the calculation of saturated liquid and saturated steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located on the saturated liquid line, x = 0 must be entered. When calculating saturated steam (saturated vapor line) x = 1 must be entered.

The calculation for x-values between 0 and 1 is not possible.

When calculating saturated liquid or saturated steam, it is adequate to enter either the given value for t <u>and</u> p = -1, or the given value for p and t = -1, plus the value for x (x = 0 or x = 1). If p and t and x are entered as given values, the program will consider p and t to be appropriate to represent the vapor pressure curve. If it is not the case the calculation for the quantity of the chosen function to be calculated results in -1000.

Saturated liquid and saturated vapor line:

Temperature range from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to  $t_{\text{c}} = 101.03 \text{ °C}$ from  $p_{\rm t} = 0.00389564$  bar to  $p_{\rm C} = 40.566$  bar Pressure range

#### Results for wrong input values

Result ETA\_PTX\_R134A, ETA = -1000 or eta\_ptx\_R134a = -1000 for input values:

p > 700 bar or p < 0.00389564 bar or Single phase region:

t > 181.85°C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  or  $\rho > 1550 \text{ m}^3 / \text{kg}$ (x = -1)

at p = -1000 and t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ Saturation lines:

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and

t > 101.03 °C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$ 

#### **References:** [16], [22]

### Specific Enthalpy h = f(p, t, x)

Function Name: h\_ptx\_R134a

Subroutine with function value: REAL\*8 FUNCTION H\_PTX\_R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_H\_PTX\_R134A(H,P,T,X)

for call from DLL: REAL\*8 H,P,T,X

#### **Input Values:**

 ${\bf P}$  - Pressure p in bar

T - Temperature t in °C

**X** - Vapor fraction *x* (kg of saturated steam)/(kg wet steam)

#### Result

**H\_PTX\_R134A**, **H** or **h\_ptx\_R134a** - Specific enthalpy *h* in kJ/kg

#### Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

#### Details on the vapor fraction x and on the calculation of wet steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located in the wet steam region, a value for x between 0 and 1 (x = 0 for saturated liquid, x = 1 for saturated steam) must be entered.

When calculating wet steam either the given value for t and p = -1000 or the given value for p and t = -1000 and in both cases the value for x between 0 and 1 must be entered.

If p and t and x are entered as given values, the program considers p and t to be appropriate to represent the vapor pressure curve. If it is not the case the calculation for the quantity of the chosen function to be calculated results in -1000.

Saturated liquid and saturated vapor line:

Temperature range from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to  $t_{\text{C}} = 101.03 \text{ °C}$ Pressure range from  $p_{\text{t}} = 0.00389564 \text{ bar to } p_{\text{C}} = 40.566 \text{ bar}$ 

#### Results for wrong input values

Result H\_PTX\_R134A, H = -1000 or eta\_ptx\_R134a = -1000 for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  or  $\rho > 1550 \text{ m}^3 / \text{kg}$ 

Saturation lines: at p = -1000 and t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ 

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and

t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ 

# Isentropic Exponent $\kappa = f(p, t, x)$

Function Name: kappa\_ptx\_R134a

Subroutine with function value: REAL\*8 FUNCTION KAP\_PTX\_R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_KAP\_PTX\_R134A(KAP,P,T,X)

for call from DLL: REAL\*8 KAP,P,T,X

#### **Input Values:**

**P** - Pressure *p* in bar

T - Temperature t in °C

**X** - Vapor fraction x (kg of saturated steam)/(kg wet steam)

#### Result

**KAP\_PTX\_R134A**, **KAP** or **kappa\_ptx\_R134a** – Isentropic exponent 
$$\kappa = \frac{w^2}{p^* v}$$

#### Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

# Details on the vapor fraction x and on the calculation of saturated liquid and saturated steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located on the saturated liquid line, x = 0 must be entered. When calculating saturated steam (saturated vapor line) x = 1 must be entered.

The calculation for x-values between 0 and 1 is not possible.

When calculating saturated liquid or saturated steam, it is adequate to enter either the given value for t and t = -1000, or the given value for t and t = -1000, plus the value for t (t = 0 or t = 1). If t and t are entered as given values, the program will consider t and t to be appropriate to represent the vapor pressure curve. If it is not the case the calculation for the quantity of the chosen function to be calculated results in -1000.

Saturated liquid and saturated vapor line:

Temperature range from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to  $t_{\text{C}} = 101.03 \text{ °C}$ Pressure range from  $p_{\text{t}} = 0.00389564 \text{ bar to } p_{\text{c}} = 40.566 \text{ bar}$ 

#### Results for wrong input values

Result KAP\_PTX\_R134A, KAP = -1000 or kappa\_ptx\_R134a = -1000 for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  or  $\rho > 1550 \text{ m}^3 / \text{kg}$ 

Saturation lines: at p = -1000 and t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ 

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ 

## Thermal Conductivity $\lambda = f(p, t, x)$

Function Name: lambda\_ptx\_R134a

Subroutine with function value: REAL\*8 FUNCTION LAM\_PTX\_R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_LAM\_PTX\_R134A(LAM,P,T,X)

for call from DLL: REAL\*8 LAM,P,T,X

#### **Input Values:**

**P** - Pressure *p* in bar **T** - Temperature *t* in °C

**X** - Vapor fraction x (kg of saturated steam)/(kg wet steam)

#### Result

**LAM\_PTX\_R134A**, **LAM** or **lambda\_ptx\_R134a** – Thermal conductivity  $\lambda$  in W / m K

#### Range of validity

Temperature range: from - 73.15 °C to 176.85 °C

Pressure range: from 0.00389564 bar to 700 bar

Density range: from  $0.00105455 \text{ kg/m}^3$  to  $1550 \text{ kg/m}^3$ 

# Details on the vapor fraction x and on the calculation of saturated liquid and saturated steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located on the saturated liquid line, x = 0 must be entered. When calculating saturated steam (saturated vapor line) x = 1 must be entered.

The calculation for x-values between 0 and 1 is not possible.

When calculating saturated liquid or saturated steam, it is adequate to enter either the given value for t and t = -1000, or the given value for t and t = -1000, plus the value for t (t = 0 or t = 1). If t and t are entered as given values, the program will consider t and t to be appropriate to represent the vapor pressure curve. If it is not the case the calculation for the quantity of the chosen function to be calculated results in -1000.

Saturated liquid and saturated vapor line:

Temperature range from t = -103.30 °C to  $t_c = 101.03$  °C

Pressure range from  $p_{\rm t} = 0.00389564$  bar to  $p_{\rm c} = 40.566$  bar

#### Results for wrong input values

Result LAM\_PTX\_R134A, LAM = - 1000 or lambda\_ptx\_R134a = -1000 for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or t < -103.3 °C or  $\rho > 1550$  m<sup>3</sup> /kg

Saturation lines: at p = -1000 and t > 101.03 °C or t < 73.15°C

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and

t > 101.03 °C or t < -103.30 °C

**References:** [16], [23]

## Kinematic Viscosity v = f(p, t, x)

Function Name: ny\_ptx\_R134a

Subroutine with function value: REAL\*8 FUNCTION NY\_PTX\_ R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_NY \_PTX\_ R134A(NY,P,T,X)

for call from DLL: REAL\*8 NY,P,T,X

#### **Input Values:**

**P** - Pressure *p* in bar **T** - Temperature *t* in °C

**X** - Vapor fraction x (kg of saturated steam)/(kg wet steam)

#### Result

```
NY_PTX_ R134A, NY or ny_ptx_ R134a - Kinematic viscosity v = \eta * v \text{ in m}^2/\text{s}
```

#### Range of validity

Temperature range: from - 73.15 °C to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

Density range: from 0.00105455 m<sup>3</sup> / kg to 1550 m<sup>3</sup> / kg

# Details on the vapor fraction *x* and on the calculation of saturated liquid and saturated steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located on the saturated liquid line, x = 0 must be entered. When calculating saturated steam (saturated vapor line) x = 1 must be entered.

The calculation for x-values between 0 and 1 is not possible.

When calculating saturated liquid or saturated steam, it is adequate to enter either the given value for t and t = -1000, or the given value for t and t = -1000, plus the value for t (t = 0 or t = 1). If t and t are entered as given values, the program will consider t and t to be appropriate to represent the vapor pressure curve. If it is not the case the calculation for the quantity of the chosen function to be calculated results in -1000.

Saturated liquid and saturated vapor line:

Temperature range from t = -103.30 °C to  $t_c = 101.03$  °C

Pressure range from  $p_t = 0.00389564$  bar to  $p_c = 40.566$  bar

#### Results for wrong input values

Result NY\_PTX\_ R134A, NY= -1000 or ny\_ptx\_ R134a = -1000 for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or t < -103.3 °C or  $\rho > 1550$  m<sup>3</sup> / kg Saturation lines: at  $\rho = -1000$  and t > 101.03 °C or t < 73.15°C

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and

at p > 40.000 bat of p < 0.0000000 bat of

*t* > 101.03 °C or *t* < -103.30 °C

**References:** [16], [22]

## Prandtl-Number Pr = f(p, t, x)

Function Name: Pr\_ptx\_R134a

Subroutine with function value: REAL\*8 FUNCTION PR PTX R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_PR \_PTX\_R134A(PR,P,T,X)

for call from DLL: REAL\*8 PR,P,T,X

#### **Input Values:**

**P** - Pressure *p* in bar

T - Temperature t in °C

**X** - Vapor fraction *x* (kg of saturated steam)/(kg wet steam)

#### Result

PR\_PTX\_R134A, PR or Pr\_ptx\_R134a - Prandtl-Number Pr = 
$$\frac{\eta^* c_p}{\lambda}$$

#### Range of validity

Temperature range: from - 73.15 °C to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

Density range: from 0.00105455 m<sup>3</sup> / kg to 1550 m<sup>3</sup> / kg

# Details on the vapor fraction x and on the calculation of saturated liquid and saturated steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located on the saturated liquid line, x = 0 must be entered. When calculating saturated steam (saturated vapor line) x = 1 must be entered.

The calculation for x-values between 0 and 1 is not possible.

When calculating saturated liquid or saturated steam, it is adequate to enter either the given value for t and t = -1000, or the given value for t and t = -1000, plus the value for t (t = 0 or t = 1). If t and t are entered as given values, the program will consider t and t to be appropriate to represent the vapor pressure curve. If it is not the case the calculation for the quantity of the chosen function to be calculated results in -1000.

Saturated liquid and saturated vapor line:

Temperature range from t = -103.30 °C to  $t_c = 101.03$  °C

Pressure range from  $p_t = 0.00389564$  bar to  $p_c = 40.566$  bar

#### Results for wrong input values

Result **PR\_PTX\_ R134A**, **PR= -1000** or **Pr\_ptx\_ R134a = -1000** for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or t < -103.3 °C or  $\rho > 1550$  m<sup>3</sup> /kg Saturation lines: at  $\rho = -1000$  and t > 101.03 °C or t < -73.15°C

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and

*t* > 101.03 °C or *t* < -103.30 °C

**References:** [16], [22], [23]

# Vapor Pressure $p_s = f(t)$

Function Name: ps\_t\_R134a

Subroutine with function value: REAL\*8 FUNCTION PS\_T\_ R134A(T)

for call from Fortran: REAL\*8 T

Subroutine with parameter: INTEGER\*4 FUNCTION C\_PS\_T\_ R134A(PS,T)

for call from DLL: REAL\*8 PS,T

#### **Input Values:**

T - Temperature t in °C

#### Result

 $PS_T_R134A$ , PS or  $ps_t_R134a$  — Vapor pressure  $p_S$  in bar

#### Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 101.03 °C

#### Results for wrong input values

Result **PS\_T\_ R134A, PS = -1000** or **ps\_t\_ R134a = -1000** for input values:

t > 101.03 °C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$ 

# Density $\rho = f(p,t,x)$

Function Name: rho\_ptx\_ R134a

Subroutine with function value: REAL\*8 FUNCTION RHO PTX R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_RHO\_PTX\_ R134A(RHO,P,T,X)

for call from DLL: REAL\*8 RHO,P,T,X

#### **Input Values:**

**P** - Pressure *p* in bar

T - Temperature t in °C

**X** - Vapor fraction x (kg of saturated steam)/(kg wet steam)

#### Result

**RHO\_PTX\_R134A**, **RHO** or **rho\_ptx\_R134a** – Density  $\rho$  in kg/m<sup>3</sup>

#### Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

#### Details on the vapor fraction x and on the calculation of wet steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located in the wet steam region, a value for x between 0 and 1 (x = 0 for saturated liquid, x = 1 for saturated steam) must be entered.

When calculating wet steam either the given value for t and p = -1000 or the given value for p and t = -1000 and in both cases the value for x between 0 and 1 must be entered.

If p and t and x are entered as given values, the program considers p and t to be appropriate to represent the vapor pressure curve. If it is not the case the calculation for the quantity of the chosen function to be calculated results in -1000.

Saturated liquid and saturated vapor line:

Temperature range from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to  $t_{\text{c}} = 101.03 \text{ °C}$ Pressure range from  $p_{\text{t}} = 0.00389564 \text{ bar to } p_{\text{c}} = 40.566 \text{ bar}$ 

#### Results for wrong input values

Result RHO\_PTX\_R134a, RHO= -1000 or rho\_ptx\_R134a = -1000 for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  or  $\rho > 1550 \text{ m}^3 / \text{kg}$ 

Saturation lines: at p = -1000 and t > 101.03 °C or t < -73.15°C

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ 

### Specific Entropy s = f(p,t,x)

Function Name: s\_ptx\_R134a

Subroutine with function value: REAL\*8 FUNCTION S\_PTX\_R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_S\_PTX\_R134A(S,P,T,X)

for call from DLL: REAL\*8 S,P,T,X

#### **Input Values:**

**P** - Pressure *p* in bar

T - Temperature t in °C

**X** - Vapor fraction x (kg of saturated steam)/(kg wet steam)

#### Result

S\_PTX\_R134A, S or s\_ptx\_R134a - Specific entropy s in kJ/kg K

#### Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

#### Details on the vapor fraction x and on the calculation of wet steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located in the wet steam region, a value for x between 0 and 1 (x = 0 for saturated liquid, x = 1 for saturated steam) must be entered.

When calculating wet steam either the given value for t and p = -1000 or the given value for p and t = -1000 and in both cases the value for x between 0 and 1 must be entered.

If p and t and x are entered as given values, the program considers p and t to be appropriate to represent the vapor pressure curve.

If it is not the case the calculation for the quantity of the chosen function to be calculated results in - 1000.

Saturated liquid and saturated vapor line:

Temperature range from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to  $t_{\text{c}} = 101.03 \text{ °C}$ Pressure range from  $p_{\text{t}} = 0.00389564$  bar to  $p_{\text{c}} = 40.566$  bar

#### Results for wrong input values

Result  $S_{PTX}_{R134A}$ , S = -1000 or  $S_{ptx}_{R134a} = -1000$  for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or t < -73.15 °C or  $\rho > 1550$  m<sup>3</sup> /kg Saturation lines: at  $\rho = -1000$  and t > 101.03 °C or t < -73.15°C

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ 

t > 101.03 C of  $t < t(p, p_{\text{max}} = 1550 \text{ k})$ 

# Surface Tension $\sigma = f(t)$

Function Name: sigma\_t\_R134a

Subroutine with function value: REAL\*8 FUNCTION SIGMA\_T\_R134A(T)

for call from Fortran: REAL\*8 T

Subroutine with parameter: INTEGER\*4 FUNCTION C\_SIGMA\_T\_R134A(SIGMA,T)

for call from DLL: REAL\*8 SIGMA,T

**Input Values:** 

T - Temperature t in °C

Result

SIGMA\_T\_R134A, SIGMA or sigma\_t\_R134a - Surface tension  $\sigma$  in N/m

Range of validity

Temperature range: from - 103.30 °C to 181.85 °C

Results for wrong input values

Result SIGMA\_T\_R134A, SIGMA= -1000 or sigma\_t\_R134a = -1000 for input values:

**References:** [16], [22]

### Backward Function: Temperature t = f(p,h)

Function Name: t\_ph\_R134a

Subroutine with function value: REAL\*8 FUNCTION T\_PH\_R134A(P,H)

for call from Fortran: REAL\*8 P,H

Subroutine with parameter: INTEGER\*4 FUNCTION C\_T \_PH\_R134A(T,P,H)

for call from DLL: REAL\*8 T,P,H

#### **Input Values:**

**P** - Pressure *p* in bar

H - Specific enthalpy h in kJ/kg

#### Result

**T\_PH\_R134A**, **T** or **t\_ph\_R134a** - Temperature *t* in °C

#### Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

#### Details on the calculation of wet steam

The wet steam region is calculated automatically. This means that from the given values of p and h the function will determine whether the state point to be calculated is located within the single-phase region (liquid or steam) or the wet steam region. Afterwards the calculation of t in the appropriate region will be carried out.

Wet steam region: Pressure ranges from  $p_t = 0.00389564$  bar to  $p_c = 40.566$  bar

#### Results for wrong input values

Result T PH R134A, T = -1000 or t ph R134a = -1000 for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  or  $\rho > 1550 \text{ m}^3 / \text{kg}$ 

Saturation lines: at p > 70.54 bar or p < 0.00389564 bar or

t > 101.03 °C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$ 

# Backward Function: Temperature t = f(p,s)

Function Name: t\_ps\_R134a

Subroutine with function value: REAL\*8 FUNCTION T\_PS\_R134A(P,S)

for call from Fortran: REAL\*8 P,S

Subroutine with parameter: INTEGER\*4 FUNCTION C\_T\_PS\_R134A(T,P,S)

for call from DLL: REAL\*8 T,P,S

# **Input Values:**

P - Pressure p in bar

S - Specific entropy s in kJ/(kg K)

# Result

T\_PS\_R134A, T or t\_ps\_R134a - Temperature t in °C

# Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

# Details on the calculation of wet steam

The wet steam region is calculated automatically. This means that from the given values of p and s the function will determine whether the state point to be calculated is located within the single-phase region (liquid or steam) or the wet steam region. Afterwards the calculation of t in the appropriate region will be carried out.

Wet steam region: Pressure ranges from  $p_{\rm r} = 0.00389564$  bar to  $p_{\rm c} = 40.566$  bar

# Results for wrong input values

Result  $T_PS_R134A$ , T = -1000 or  $t_ps_R134a = -1000$  for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$  or  $\rho > 1550 \text{ m}^3 / \text{kg}$ 

Saturation lines: at p > 70.54 bar or p < 0.00389564 bar or

t > 101.03 °C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$ 

# Saturation Temperature $t_s = f(p)$

Function Name: ts\_p\_R134a

Subroutine with function value: REAL\*8 FUNCTION TS\_P\_R134A(P)

for call from Fortran: REAL\*8 P

Subroutine with parameter: INTEGER\*4 FUNCTION C\_TS\_P\_R134A(TS,P)

for call from DLL: REAL\*8 TS,P

**Input Values:** 

**P** - Pressure *p* in bar

Result

**TS\_P\_R134A**, **TS** or **ts\_p\_R134a** – Saturation temperature  $t_S$  in °C

Range of validity

Pressure range: from 0.00389564 bar to 40.566 bar

Results for wrong input values

Result TS\_P\_R134A, TS = -1000 or ts\_p\_R134a = -1000 for input values:

p < 0.00389564 bar or p > 40.566 bar

# Specific Internal Energy u = f(p,t,x)

Function Name: u\_ptx\_R134a

Subroutine with function value: REAL\*8 FUNCTION U\_PTX\_R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_U\_PTX\_R134A(U,P,T,X)

for call from DLL: REAL\*8 U,P,T,X

# **Input Values:**

P - Pressure p in bar

T - Temperature t in °C

**X** - Vapor fraction x (kg of saturated steam)/(kg wet steam)

#### Result

**U\_PTX\_R134A**, **U** or **u\_ptx\_R134a** - Specific internal energy *u* in kJ/kg

# Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

# Details on the vapor fraction x and on the calculation of wet steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located in the wet steam region, a value for x between 0 and 1 (x = 0 for saturated liquid, x = 1 for saturated steam) must be entered.

When calculating wet steam either the given value for t and p = -1000 or the given value for p and t = -1000 and in both cases the value for x between 0 and 1 must be entered.

If p and t and x are entered as given values, the program considers p and t to be appropriate to represent the vapor pressure curve. If it is not the case the calculation for the quantity of the chosen function to be calculated results in -1000.

Saturated liquid and saturated vapor line:

Temperature range from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to  $t_{\text{c}} = 101.03 \text{ °C}$ Pressure range from  $p_{\text{t}} = 0.00389564$  bar to  $p_{\text{c}} = 40.566$  bar

# Results for wrong input values

Result **U PTX R134A**, **U = -1000** or **u ptx R134a = -1000** for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  or  $\rho > 1550 \text{ m}^3 / \text{kg}$ 

Saturation lines: at p = -1000 and t > 101.03 °C or t < -73.15°C

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ 

# Specific Volume v = f(p, t, x)

Function Name: v\_ptx\_R134a

Subroutine with function value: REAL\*8 FUNCTION V\_PTX\_R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_V\_PTX\_R134A(V,P,T,X)

for call from DLL: REAL\*8 V,P,T,X

# **Input Values:**

**P** - Pressure *p* in bar

T - Temperature t in °C

**X** - Vapor fraction x (kg of saturated steam)/(kg wet steam)

#### Result

 $V_PTX_R134A$ , V or  $v_ptx_R134a$  – Specific volume v in  $m^3$  /kg

# Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

# Details on the vapor fraction x and on the calculation of wet steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located in the wet steam region, a value for x between 0 and 1 (x = 0 for saturated liquid, x = 1 for saturated steam) must be entered.

When calculating wet steam either the given value for t and p = -1000 or the given value for p and t = -1000 and in both cases the value for x between 0 and 1 must be entered.

If p and t and x are entered as given values, the program considers p and t to be appropriate to represent the vapor pressure curve. If it is not the case the calculation for the quantity of the chosen function to be calculated results in -1000.

Saturated liquid and saturated vapor line:

Temperature range from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to  $t_{\text{c}} = 101.03 \text{ °C}$ Pressure range from  $p_{\text{t}} = 0.00389564 \text{ bar to } p_{\text{c}} = 40.566 \text{ bar}$ 

### Results for wrong input values

Result  $V_PTX_R134A$ , V = -1000 or  $v_ptx_R134a = -1000$  for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$  or  $\rho > 1550 \text{ m}^3 / \text{kg}$ 

Saturation lines: at p = -1000 and t > 101.03 °C or t < -73.15°C

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ 

# Isentropic Speed of Sound w = f(p,t,x)

Function Name: w\_ptx\_R134a

Subroutine with function value: REAL\*8 FUNCTION W\_PTX\_R134A(P,T,X)

for call from Fortran: REAL\*8 P,T,X

Subroutine with parameter: INTEGER\*4 FUNCTION C\_W\_PTX\_R134A(W,P,T,X)

for call from DLL: REAL\*8 W,P,T,X

# **Input Values:**

**P** - Pressure *p* in bar

T - Temperature t in °C

**X** - Vapor fraction *x* (kg of saturated steam)/(kg wet steam)

#### Result

W\_PTX\_R134A, W or w\_ptx\_R134a - Speed of sound w in m/s

# Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

# Details on the vapor fraction x and on the calculation of saturated liquid and saturated steam

The wet steam region is calculated automatically by the subprograms. For this purpose the following fixed details on the vapor fraction *x* are to be considered:

If the state point to be calculated is located in the single-phase region (liquid or superheated steam) x = -1 must be entered as a pro-forma value.

If the state point to be calculated is located on the saturated liquid line, x = 0 must be entered. When calculating saturated steam (saturated vapor line) x = 1 must be entered.

The calculation for x-values between 0 and 1 is not possible.

When calculating saturated liquid or saturated steam, it is adequate to enter either the given value for t and p = -1000, or the given value for p and t = -1000, plus the value for x (x = 0 or x = 1). If p and t and t are entered as given values, the program will consider p and t to be appropriate to represent the vapor pressure curve.

Saturated liquid and saturated vapor line:

Temperature range from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to  $t_{\text{c}} = 101.03 \text{ °C}$ Pressure range from  $p_{\text{t}} = 0.00389564 \text{ bar to } p_{\text{c}} = 40.566 \text{ bar}$ 

### Results for wrong input values

Result W PTX R134A, W = -1000 or w ptx R134a = -1000 for input values:

Single phase region: p > 700 bar or p < 0.00389564 bar or

(x = -1) t > 181.85°C or  $t < t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  or  $\rho > 1550 \text{ m}^3 / \text{kg}$ 

Saturation lines: at p = -1000 and t > 101.03 °C or t < -73.15°C

at t = -1000 and p > 40.566 bar or p < 0.00389564 bar or

at p > 40.566 bar or p < 0.00389564 bar and t > 101.03 °C or  $t < t(p, \rho_{max} = 1550 \text{ kg/m}^3)$ 

# Backward Function: Vapor Fraction x = f(p,h)

Function Name: x\_ph\_R134a

Subroutine with function value: REAL\*8 FUNCTION X\_PH\_R134A(P,H)

for call from Fortran: REAL\*8 P,H

Subroutine with parameter: INTEGER\*4 FUNCTION C\_X\_PH\_R134A(T,P,H)

for call from DLL: REAL\*8 X,P,H

# **Input Values:**

P - Pressure p in bar

H - Specific enthalpy h in kJ/kg

# Result

**X\_PH\_R134A**, **X** or **x\_ph\_R134a** - Vapor fraction *x* in (kg saturated steam/kg wet steam)

# Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 181.85 °C

Pressure range: from 0.00389564 bar to 700 bar

#### Details on the calculation of wet steam

The wet steam region is calculated automatically. This means that from the given values of v and u the function will determine whether the state point to be calculated is located within the single-phase region (liquid or steam) or the wet steam region. When calculating wet steam the value for x between 0 and 1 is calculated (0 for saturated liquid, 1 for saturated steam). If the state point to be calculated is located in the single-phase region the result x = -1 will be returned.

Wet steam region: Pressure ranges from  $p_{\rm t} = 0.00389564$  bar to  $p_{\rm c} = 40.566$  bar

# Results for wrong input values

Result  $X_PH_R134A$ , X = -1 or  $x_ph_R134a = -1$  for input values:

In case the state point is located in the single phase region

p < 40.566 bar or p > 0.00389564 bar

# Backward Function: Vapor Fraction x = f(p,s)

Function Name: x\_ps\_R134a

Subroutine with function value: REAL\*8 FUNCTION X\_PS\_R134A(P,S)

for call from Fortran: REAL\*8 P,S

Subroutine with parameter: INTEGER\*4 FUNCTION C\_X\_PS\_R134A(X,P,S)

for call from DLL: REAL\*8 X,P,S

# **Input Values:**

P - Pressure p in bar

S - Specific entropy s in kJ/(kg K)

# Result

X\_PS\_R134A, X or x\_ps\_R134a - Vapor fraction x in (kg saturated steam/kg wet steam)

# Range of validity

Temperature range: from  $t(p, \rho_{\text{max}} = 1550 \text{ kg/m}^3)$  to 101.03 °C

Pressure range: from 0.00389564 bar to 700 bar

#### Details on the calculation of wet steam

The wet steam region is calculated automatically. This means that from the given values of p and s the function will determine whether the state point to be calculated is located within the single-phase region (liquid or steam) or the wet steam region. When calculating wet steam the value for x between 0 and 1 is calculated (0 for saturated liquid, 1 for saturated steam). If the state point to be calculated is located in the single-phase region the result x = -1 will be returned.

Wet steam region: Pressure ranges from  $p_t = 0.00389564$  bar to  $p_c = 40.566$  bar

# Results for wrong input values

Result  $X_PS_R134A$ , X = -1 or  $x_ps_R134a = -1$  for input values:

In case the state point is located in the single phase region

p < 40.566 bar or p > 0.00389564 bar



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Department of Technical Thermodynamics www.thermodynamics-zittau.de



# **Property Libraries** for Calculating Heat Cycles, Boilers, Turbines and Refrigerators

#### Water and Steam

# **Library LibIF97**

- Industrial Formulation IAPWS-IF97 (Revision 2007)
- Supplementary Standards
- IAPWS-IF97-S01
- IAPWS-IF97-S03rev
- IAPWS-IF97-S04
- IAPWS-IF97-S05
- IAPWS Revised Advisory Note No. 3 on Thermodynamic Derivatives (2008)

#### **Humid Combustion Gas Mixtures**

# Library LibHuGas

Model: Ideal mixture of the real fluids:

CO<sub>2</sub> - Span and Wagner O<sub>2</sub> - Schmidt and Wagner

H<sub>2</sub>O - IAPWS-95 Ar - Tegeler et al.

N<sub>2</sub> - Span et al.

and of the ideal gases:

SO<sub>2</sub>, CO, Ne (Scientific Formulation of Bücker et al.)

Consideration of:

Dissociation from VDI 4670 and Poynting effect

# **Humid Air**

# Library LibHuAir

Model: Ideal mixture of the real fluids:

- Dry Air from Lemmon et al.
- Steam, water and ice from IAPWS-IF97 and IAPWS-06

#### Consideration of:

- Condensation and freezing of steam
- Dissociation from the VDI 4670
- Poynting effect from ASHRAE RP-1485

# Carbon Dioxide including Dry Ice Library LibCO2

Formulation of Span and Wagner (1994)

### Seawater

# Library LibSeaWa

IAPWS Industrial Formulation 2013

# Ice

# **Library LibICE**

Ice from IAPWS-06, Melting and sublimation pressures from IAPWS-08, Water from IAPWS-IF97, Steam from IAPWS-95 and -IF97

#### **Ideal Gas Mixtures**

# Library LibldGasMix

Model: Ideal mixture of the ideal gases:

Αſ	NO	не	Propylene
Ne	H <sub>2</sub> O	$F_2$	Propane
$N_2$	SO <sub>2</sub>	NH <sub>3</sub>	Iso-Butane
$O_2$	H <sub>2</sub>	Methane	n-Butane
CO	H₂S	Ethane	Benzene
CO <sub>2</sub>	OH	Ethylene	Methanol
Air			

Consideration of:

Dissociation from the VDI Guideline 4670

# **Library LibIDGAS**

Model: Ideal gas mixture from VDI Guideline 4670

Consideration of:

• Dissociation from the VDI Guideline 4670

# Dry Air including Liquid Air Library LibRealAir

Formulation of Lemmon et al. (2000)

# Nitrogen

# Library LibN2

Formulation of Span et al. (2000)

# Hydrogen

# **Library LibH2**

Formulation of Leachman et al. (2007)

# Refrigerants

# Ammonia

# **Library LibNH3**

Formulation of Tillner-Roth (1995)

R134a

# Library LibR134a

Formulation of Tillner-Roth and Baehr (1994)

Iso-Butane

# Library LibButane\_Iso

Formulation of Bücker et al. (2003)

n-Butane

# Library LibButane\_n

Formulation of Bücker et al. (2003)

# **Mixtures for Absorption Processes**

# Ammonia/Water Mixtures

# **Library LibAmWa**

IAPWS Guideline 2001 of Tillner-Roth and Friend (1998)

Helmholtz energy equation for the mixing term
(also useable for calculating Kalina Cycle)

#### Water/Lithium Bromide Mixtures

# Library LibWaLi

Formulation of Kim and Infante Ferreira (2004)
Gibbs energy equation for the mixing term

# **Liquid Coolants**

# Liquid Secondary Refrigerants

### Library LibSecRef

Liquid solutions of water with

 $C_2H_6O_2$  Ethylene glycol  $C_3H_8O_2$  Propylene glycol  $C_2H_5OH$  Ethyl alcohol  $CH_3OH$  Methyl alcohol  $C_2H_9O_3$  Glycerol

K<sub>2</sub>CO<sub>3</sub> Glycerol Potassium carbonate

CaCl<sub>2</sub> Calcium chloride
MgCl<sub>2</sub> Magnesium chloride
NaCl Sodium chloride

NaCl Sodium chloride C<sub>2</sub>H<sub>3</sub>KO<sub>2</sub> Potassium acetate

Formulation of the International Institute of Refrigeration (1997)

# Siloxanes as ORC Working Fluids

Octamethylcyclotetrasiloxane C<sub>8</sub>H<sub>24</sub>O<sub>4</sub>Si<sub>4</sub> Library LibD4

Decamethylcyclopentasiloxane C<sub>10</sub>H<sub>30</sub>O<sub>5</sub>Si<sub>5</sub> Library LibD5

Tetradecamethylhexasiloxane C<sub>14</sub>H<sub>42</sub>O<sub>5</sub>Si<sub>6</sub> Library LibMD4M

Hexamethyldisiloxane C<sub>6</sub>H<sub>18</sub>OSi<sub>2</sub> Library LibMM

Formulation of Colonna et al. (2006)

Dodecamethylcyclohexasiloxane C<sub>12</sub>H<sub>36</sub>O<sub>6</sub>Si<sub>6</sub> Library LibD6

Decamethyltetrasiloxane C<sub>10</sub>H<sub>30</sub>O<sub>3</sub>Si<sub>4</sub> Library LibMD2M

Dodecamethylpentasiloxane C<sub>12</sub>H<sub>36</sub>O<sub>4</sub>Si<sub>5</sub> Library LibMD3M

Octamethyltrisiloxane C<sub>8</sub>H<sub>24</sub>O<sub>2</sub>Si<sub>3</sub> Library LibMDM

Formulation of Colonna et al. (2008)

# **Propane**

# **Library LibPropane**

Formulation of Lemmon et al. (2007)

# Methanol

# **Library LibCH3OH**

Formulation of de Reuck and Craven (1993)

# **Ethanol**

# Library LibC2H5OH

Formulation of Schroeder et al. (2012)

# Helium Library LibHe

Formulation of Arp et al. (1998)

# **Hydrocarbons**

Decane C<sub>10</sub>H<sub>22</sub> Library LibC10H22

Isopentane C<sub>5</sub>H<sub>12</sub> Library LibC5H12\_ISO

Neopentane C<sub>5</sub>H<sub>12</sub> Library LibC5H12\_NEO

Isohexane C<sub>6</sub>H<sub>14</sub> Library LibC6H14

Toluene C<sub>7</sub>H<sub>8</sub> Library LibC7H8

Formulation of Lemmon and Span (2006)

# **Further Fluids**

Carbon monoxide CO Library LibCO

Carbonyl sulfide COS Library LibCOS

Hydrogen sulfide H<sub>2</sub>S Library LibH2S

Dinitrogen monooxide N<sub>2</sub>O Library LibN2O

Sulfur dioxide SO<sub>2</sub> Library LibSO2

Acetone C<sub>3</sub>H<sub>6</sub>O Library LibC3H6O

Formulation of Lemmon and Span (2006)

# For more information please contact:

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Phone: +49-3583-61-1846 Fax.: +49-3583-61-1846

# The following thermodynamic and transport properties can be calculated<sup>a</sup>:

# Thermodynamic Properties

- Vapor pressure p<sub>s</sub>
- Saturation temperature T<sub>s</sub>
- Density  $\rho$
- Specific volume v
- Enthalpy h
- Internal energy u
- Entropy s
- Exergy e
- Isobaric heat capacity  $c_{p}$
- Isochoric heat capacity c<sub>v</sub>
- Isentropic exponent κ
  Speed of sound w
- Surface tension σ

# **Transport Properties**

- $\bullet$  Dynamic viscosity  $\eta$
- ullet Kinematic viscosity u
- $\bullet$  Thermal conductivity  $\lambda$
- Prandtl-number Pr

# **Backward Functions**

- T, v, s (p,h)
- T, v, h (p,s)
- p, T, v (h,s)
- p, T (v,h)
- p, T (v,u)

# Thermodynamic Derivatives

Partial derivatives can be calculated.

<sup>&</sup>lt;sup>a</sup> Not all of these property functions are available in all property libraries.

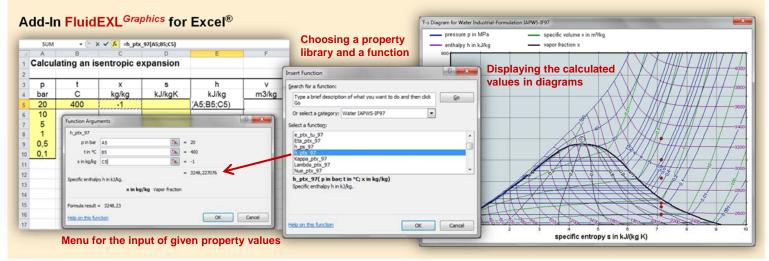


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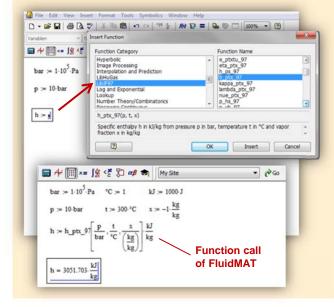


# **Property Software for Calculating Heat Cycles, Boilers, Turbines and Refrigerators**



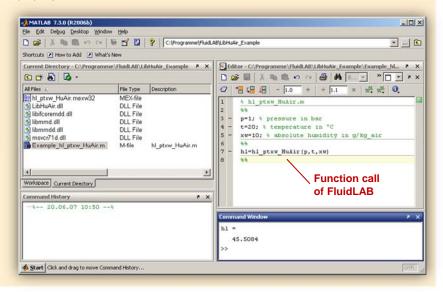
# Add-In FluidMAT for Mathcad®

The property libraries can be used in Mathcad®.



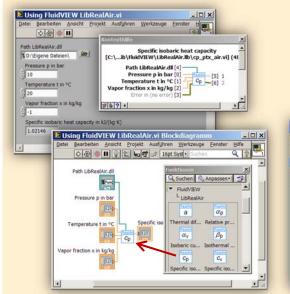
# Add-In FluidLAB for MATLAB®

Using the Add-In FluidLAB the property functions can be called in MATLAB®.



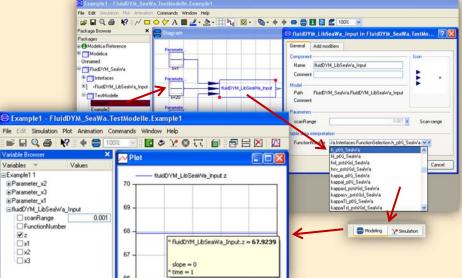
# Add-On FluidVIEW for LabVIEW®

The property functions can be calculated in LabVIEW®.

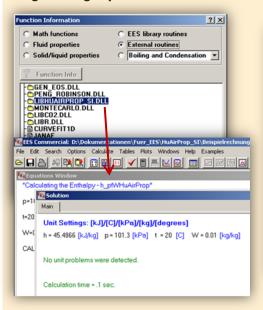


# Add-In FluidDYM for DYMOLA® (Modelica) and SimulationX®

The property functions can be called in DYMOLA® and SimulationX®



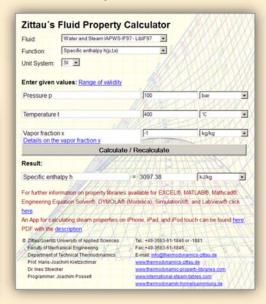
# Add-In FluidEES for Engineering Equation Solver®



# App International Steam Tables for iPhone, iPad, iPod touch, Android smart phones and tablets



# Online Property Calculator at www.thermodynamics-zittau.de



# **Property Software for Pocket Calculators**







# For more information please contact:

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Phone: +49-3583-61-1846 Fax.: +49-3583-61-1846

The following thermodynamic and transport properties<sup>a</sup> can be calculated in Excel<sup>®</sup>, MATLAB<sup>®</sup>, Mathcad<sup>®</sup>, Engineering Equation Solver<sup>®</sup> EES, DYMOLA<sup>®</sup> (Modelica), SimulationX<sup>®</sup>, and LabVIEW<sup>®</sup>:

### Thermodynamic Properties

- Vapor pressure  $p_s$
- Saturation temperature T<sub>s</sub>
- $\bullet \ {\rm Density} \ \rho$
- · Specific volume v
- Enthalpy h
- Internal energy u
- Entropy s
- Exergy e
- Isobaric heat capacity c<sub>p</sub>
- Isochoric heat capacity c<sub>v</sub>
- Isentropic exponent  $\kappa$
- Speed of sound w
- Surface tension σ

### **Transport Properties**

- Dynamic viscosity  $\eta$
- Kinematic viscosity v
- Thermal conductivity  $\lambda$
- Thermal conductivity
- Prandtl-number Pr

# **Backward Functions**

- T, v, s (p,h)
- T, v, h (p,s)
- p, T, v (h,s)
- p, T (v,h)
- p, T (v,u)

#### Thermodynamic Derivatives

 Partial derivatives can be calculated.

<sup>&</sup>lt;sup>a</sup> Not all of these property functions are available in all property libraries.

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# 6. Satisfied Customers

Date: 04/2014

The following companies and institutions use the property libraries

- FluidEXL<sup>Graphics</sup> for Excel<sup>®</sup>
- FluidLAB for MATLAB®
- FluidMAT for Mathcad®
- FluidEES for Engineering Equation Solver® EES
- FluidDYM for Dymola  $^{\mbox{\scriptsize R}}$  (Modelica) and Simulation  $X^{\mbox{\scriptsize R}}$
- FluidVIEW for LabVIEW®:

# 2014

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Technical University of Vienna, Austria	04/2014
MTU Aero Engines AG, Munich	04/2014
GKS, Schweinfurt	03/2014
Technical University of Nurnberg	03/2014
EP-E, Niederstetten	03/2014
Rückert NatUrgas GmbH, Lauf	03/2014
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	SPG, Montreuil Cedex, France	02/2012
	German Destilation, Sprendlingen	02/2012
	Lopez, Munguia, Spain	02/2012
	Endress & Hauser, Hannover	02/2012
	Palo Alto Research Center, USA	02/2012
	WIPAK, Walsrode	02/2012
	Freudenberg, Weinheim	01/2012
	Fichtner, Stuttgart	01/2012
	airinotec, Bayreuth	01/2012, 07/2012
	University Auckland, New Zealand	01/2012
	VPC, Vetschau	01/2012
	Franken Guss, Kitzingen	01/2012
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	XRG-Simulation, Hamburg	12/2011
	Smurfit Kappa PPT, AX Roermond, Netherlands	12/2011
	AWTEC, Zurich, Switzerland	12/2011
	eins-energie, Bad Elster	12/2011
	BeNow, Rodenbach	11/2011
	Luzern University of Applied Sciences, Switzerland	11/2011
	GMVA, Oberhausen	11/2011
	CCI, Karlsruhe	10/2011
	WBüchner University of Applied Sciences, Pfungstadt	10/2011
	PLANAIR, La Sagne, Switzerland	10/2011
	LAWI, Dresden	10/2011
	Lopez, Munguia, Spain	10/2011
	University of KwaZulu-Natal, Westville, South Africa	10/2011
	Voith, Heidenheim	09/2011
	SpgBe Montreal, Canada	09/2011
	SPG TECH, Montreuil Cedex, France	09/2011
	Voith, Heidenheim-Mergelstetten	09/2011
	MTU Aero Engines, Munich	08/2011
	MIBRAG, Zeitz	08/2011
	RWE, Essen	07/2011
	Fels, Elingerode	07/2011

Weihenstephan University of Applied Sciences	07/2011, 09/2011 10/2011
Forschungszentrum Juelich	07/2011
RWTH Aachen University	07/2011, 08/2011
INNEO Solutions, Ellwangen	06/2011
Caliqua, Basel, Switzerland	06/2011
Technical University of Freiberg	06/2011
Fichtner IT Consulting, Stuttgart	05/2011, 06/2011, 08/2011
Salzgitter Flachstahl, Salzgitter	05/2011
Helbling Beratung & Bauplanung, Zurich, Switzerland	05/2011
INEOS, Cologne	04/2011
Enseleit Consulting Engineers, Siebigerode	04/2011
Witt Consulting Engineers, Stade	03/2011
Helbling, Zurich, Switzerland	03/2011
MAN Diesel, Copenhagen, Denmark	03/2011
AGO, Kulmbach	03/2011
University of Duisburg	03/2011, 06/2011
CCP, Marburg	03/2011
BASF, Ludwigshafen	02/2011
ALSTOM Power, Baden, Switzerland	02/2011
Universität der Bundeswehr, Munich	02/2011
Calorifer, Elgg, Switzerland	01/2011
STRABAG, Vienna, Austria	01/2011
TUEV Sued, Munich	01/2011
ILK Dresden	01/2011
Technical University of Dresden	01/2011, 05/2011 06/2011, 08/2011
2010	
Umweltinstitut Neumarkt	12/2010
YIT Austria, Vienna, Austria	12/2010
MCI Innsbruck, Austria	12/2010
University of Stuttgart	12/2010
HS Cooler, Wittenburg	12/2010
Visteon, Novi Jicin, Czech Republic	12/2010
CompuWave, Brunntal	12/2010

Stadtwerke Leipzig	12/2010
MCI Innsbruck, Austria	12/2010
EVONIK Energy Services, Zwingenberg	12/2010
Caliqua, Basel, Switzerland	11/2010
Shanghai New Energy Resources Science & Technology, China	11/2010
Energieversorgung Halle	11/2010
Hochschule für Technik Stuttgart, University of Applied Sciences	11/2010
Steinmueller, Berlin	11/2010
Amberg-Weiden University of Applied Sciences	11/2010
AREVA NP, Erlangen	10/2010
MAN Diesel, Augsburg	10/2010
KRONES, Neutraubling	10/2010
Vaillant, Remscheid	10/2010
PC Ware, Leipzig	10/2010
Schubert Consulting Engineers, Weißenberg	10/2010
Fraunhofer Institut UMSICHT, Oberhausen	10/2010
Behringer Consulting Engineers, Tagmersheim	09/2010
Saacke, Bremen	09/2010
WEBASTO, Neubrandenburg	09/2010
Concordia University, Montreal, Canada	09/2010
Compañía Eléctrica de Sochagota, Bogota, Colombia	08/2010
Hannover University of Applied Sciences	08/2010
ERGION, Mannheim	07/2010
Fichtner IT Consulting, Stuttgart	07/2010
TF Design, Matieland, South Africa	07/2010
MCE, Berlin	07/2010, 12/2010
IPM, Zittau/Goerlitz University of Applied Sciences	06/2010
TUEV Sued, Dresden	06/2010
RWE IT, Essen	06/2010
Glen Dimplex, Kulmbach	05/2010, 07/2010 10/2010
Hot Rock, Karlsruhe	05/2010
Darmstadt University of Applied Sciences	05/2010
Voith, Heidenheim	04/2010
CombTec, Zittau	04/2010

	University of Glasgow, Great Britain	04/2010
	Universitaet der Bundeswehr, Munich	04/2010
	Technical University of Hamburg-Harburg	04/2010
	Vattenfall Europe, Berlin	04/2010
	HUBER Consulting Engineers, Berching	04/2010
	VER, Dresden	04/2010
	CCP, Marburg	03/2010
	Offenburg University of Applied Sciences	03/2010
	Technical University of Berlin	03/2010
	NIST Boulder CO, USA	03/2010
	Technical University of Dresden	02/2010
	Siemens Energy, Nuremberg	02/2010
	Augsburg University of Applied Sciences	02/2010
	ALSTOM Power, Baden, Switzerland	02/2010, 05/2010
	MIT Massachusetts Institute of Technology Cambridge MA, USA	02/2010
	Wieland Werke, Ulm	01/2010
	Siemens Energy, Goerlitz	01/2010, 12/2010
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	ILK, Dresden	01/2010, 12/2010
	Fischer-Uhrig Consulting Engineers, Berlin	01/2010
2	009	
	ALSTOM Power, Baden, Schweiz	01/2009, 03/2009
	,	05/2009
	Nordostschweizerische Kraftwerke AG, Doettingen, Switzerland	02/2009
	RWE, Neurath	02/2009
	Brandenburg University of Technology, Cottbus	02/2009
	Hamburg University of Applied Sciences	02/2009
	Kehrein, Moers	03/2009
	EPP Software, Marburg	03/2009
	Bernd Münstermann, Telgte	03/2009
	Suedzucker, Zeitz	03/2009
	CPP, Marburg	03/2009
	Gelsenkirchen University of Applied Sciences	04/2009
	Regensburg University of Applied Sciences	05/2009
	Gatley & Associates, Atlanta, USA	05/2009

	BOSCH, Stuttgart	06/2009, 07/2009
	Dr. Nickolay, Consulting Engineers, Gommersheim	06/2009
	Ferrostal Power, Saarlouis	06/2009
	BHR Bilfinger, Essen	06/2009
	Intraserv, Wiesbaden	06/2009
	Lausitz University of Applied Sciences, Senftenberg	06/2009
	Nuernberg University of Applied Sciences	06/2009
	Technical University of Berlin	06/2009
	Fraunhofer Institut UMSICHT, Oberhausen	07/2009
	Bischoff, Aurich	07/2009
	Fichtner IT Consulting, Stuttgart	07/2009
	Techsoft, Linz, Austria	08/2009
	DLR, Stuttgart	08/2009
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	RWTH Aachen University	09/2009
	Vattenfall, Hamburg	10/2009
	AIC, Chemnitz	10/2009
	Midiplan, Bietigheim-Bissingen	11/2009
	Institute of Air Handling and Refrigeration ILK, Dresden	11/2009
	FZD, Rossendorf	11/2009
	Techgroup, Ratingen	11/2009
	Robert Sack, Heidelberg	11/2009
	EC, Heidelberg	11/2009
	MCI, Innsbruck, Austria	12/2009
	Saacke, Bremen	12/2009
	ENERKO, Aldenhoven	12/2009
20	008	
	Pink, Langenwang	01/2008
	Fischer-Uhrig, Berlin	01/2008
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	MAAG, Kuesnacht, Switzerland	02/2008
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	Rerum Cognitio, Zwickau	04/2008,	05/2008
	ARUP, Berlin		05/2008
	Research Center, Karlsruhe		07/2008
	AWECO, Neukirch		07/2008
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	Technical University of Cottbus, Chair in Power Plant Engineering	07/2008,	10/2008
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	Technip Benelux BV, Zoetermeer, Netherlands		08/2008
	Fennovoima Oy, Helsinki, Finland		08/2008
	Fichtner Consulting & IT, Stuttgart		09/2008
	PEU, Espenhain		09/2008
	Poyry, Dresden		09/2008
	WINGAS, Kassel		09/2008
	TUEV Sued, Dresden		10/2008
	Technical University of Dresden, Professorship of Thermic Energy Machines and Plants	10/2008,	11/2008
	AWTEC, Zurich, Switzerland		11/2008
	Siemens Power Generation, Erlangen		12/2008
20	007		
	Audi, Ingolstadt		02/2007
	ANO Abfallbehandlung Nord, Bremen		02/2007
	TUEV NORD SysTec, Hamburg		02/2007
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	Technical University of Dresden, Chair in Jet Propulsion Systems		02/2007
	Redacom, Nidau, Switzerland		02/2007
	Universität der Bundeswehr, Munich		02/2007
	Maxxtec, Sinsheim		03/2007
	University of Rostock, Chair in Technical Thermodynamics		03/2007
	AGO, Kulmbach		03/2007
	University of Stuttgart, Chair in Aviation Propulsions		03/2007
	Siemens Power Generation, Duisburg		03/2007

ENTHAL Haustechnik, Rees	05/2007
AWECO, Neukirch	05/2007
ALSTOM, Rugby, Great Britain	06/2007
SAAS, Possendorf	06/2007
Grenzebach BSH, Bad Hersfeld	06/2007
Reichel Engineering, Haan	06/2007
Technical University of Cottbus, Chair in Power Plant Engineering	06/2007
Voith Paper Air Systems, Bayreuth	06/2007
Egger Holzwerkstoffe, Wismar	06/2007
Tissue Europe Technologie, Mannheim	06/2007
Dometic, Siegen	07/2007
RWTH Aachen University, Institute for Electrophysics	09/2007
National Energy Technology Laboratory, Pittsburg, USA	10/2007
Energieversorgung Halle	10/2007
AL-KO, Jettingen	10/2007
Grenzebach BSH, Bad Hersfeld	10/2007
Wiesbaden University of Applied Sciences, Department of Engineering Sciences	10/2007
Endress+Hauser Messtechnik, Hannover	11/2007
Munich University of Applied Sciences, Department of Mechanical Engineering	11/2007
Rerum Cognitio, Zwickau	12/2007
Siemens Power Generation, Erlangen	11/2007
University of Rostock, Chair in Technical Thermodynamics	11/2007, 12/2007
2006	
STORA ENSO Sachsen, Eilenburg	01/2006
Technical University of Munich, Chair in Energy Systems	01/2006
NUTEC Engineering, Bisikon, Switzerland	01/2006, 04/2006
Conwel eco, Bochov, Czech Republic	01/2006
Offenburg University of Applied Sciences	01/2006
KOCH Transporttechnik, Wadgassen	01/2006
BEG Bremerhavener Entsorgungsgesellschaft	02/2006
Deggendorf University of Applied Sciences, Department of Mechanical Engineering and Mechatronics	02/2006
University of Stuttgart, Department of Thermal Fluid Flow Engines	02/2006

Technical University of Munich, Chair in Apparatus and Plant Engineering	02/2006
Energietechnik Leipzig (company license),	02/2006
Siemens Power Generation, Erlangen	02/2006, 03/2006
RWE Power, Essen	03/2006
WAETAS, Pobershau	04/2006
Siemens Power Generation, Goerlitz	04/2006
Technical University of Braunschweig, Department of Thermodynamics	04/2006
EnviCon & Plant Engineering, Nuremberg	04/2006
Brassel Engineering, Dresden	05/2006
University of Halle-Merseburg, Department of USET Merseburg incorporated society	05/2006
Technical University of Dresden, Professorship of Thermic Energy Machines and Plants	05/2006
Fichtner Consulting & IT Stuttgart (company licenses and distribution)	05/2006
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M&M Turbine Technology, Bielefeld	06/2006
Feistel Engineering, Volkach	07/2006
ThyssenKrupp Marine Systems, Kiel	07/2006
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Konstanz University of Applied Sciences, Course of Studies Construction and Development	10/2006
Siemens Power Generation, Duisburg	10/2006
Hannover University of Applied Sciences, Department of Mechanical Engineering	10/2006
Siemens Power Generation, Berlin	11/2006
Zikesch Armaturentechnik, Essen	11/2006
Wismar University of Applied Sciences, Seafaring Department	11/2006
BASF, Schwarzheide	12/2006
Enertech Energie und Technik, Radebeul	12/2006
2005	
TUEV Nord, Hannover	01/2005
J.H.K Plant Engineering and Service, Bremerhaven	01/2005
Electrowatt-EKONO, Zurich, Switzerland	01/2005

FCIT, Stuttgart	01/2005	
Energietechnik Leipzig (company license)	02/2005, 04/2005 07/2005	
eta Energieberatung, Pfaffenhofen	02/2005	
FZR Forschungszentrum, Rossendorf/Dresden	04/2005	
University of Saarbruecken	04/2005	
Technical University of Dresden Professorship of Thermic Energy Machines and Plants	04/2005	
Grenzebach BSH, Bad Hersfeld	04/2005	
TUEV Nord, Hamburg	04/2005	
Technical University of Dresden, Waste Management	05/2005	
Siemens Power Generation, Goerlitz	05/2005	
Duesseldorf University of Applied Sciences, Department of Mechanical Engineering and Process Engineering	05/2005 g	
Redacom, Nidau, Switzerland	06/2005	
Dumas Verfahrenstechnik, Hofheim	06/2005	
Alensys Engineering, Erkner	07/2005	
Stadtwerke Leipzig	07/2005	
SaarEnergie, Saarbruecken	07/2005	
ALSTOM ITC, Rugby, Great Britain	08/2005	
Technical University of Cottbus, Chair in Power Plant Engineering	ng 08/2005	
Vattenfall Europe, Berlin (group license)	08/2005	
Technical University of Berlin	10/2005	
Basel University of Applied Sciences, Department of Mechanical Engineering, Switzerland	10/2005	
Midiplan, Bietigheim-Bissingen	11/2005	
Technical University of Freiberg, Chair in Hydrogeology	11/2005	
STORA ENSO Sachsen, Eilenburg	12/2005	
Energieversorgung Halle (company license)	12/2005	
KEMA IEV, Dresden	12/2005	
2004		
Vattenfall Europe (group license)	01/2004	
TUEV Nord, Hamburg	01/2004	
University of Stuttgart, Institute of Thermodynamics and Heat En	igineering 02/2004	
MAN B&W Diesel A/S, Copenhagen, Denmark	02/2004	
Siemens AG Power Generation, Erlangen	02/2004	

	Ulm University of Applied Sciences	03/2004
	Visteon, Kerpen	03/2004, 10/2004
	Technical University of Dresden,	
	Professorship of Thermic Energy Machines and Plants	04/2004
	Rerum Cognitio, Zwickau	04/2004
	University of Saarbruecken	04/2004
	Grenzebach BSH, Bad Hersfeld	04/2004
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	HEW-Kraftwerk, Tiefstack	06/2004
	h s energieanlagen, Freising	07/2004
	FCIT, Stuttgart	08/2004
	Physikalisch Technische Bundesanstalt (PTB), Braunschweig	08/2004
	Mainova Frankfurt	08/2004
	Rietschle Energieplaner, Winterthur, Switzerland	08/2004
	MAN Turbo Machines, Oberhausen	09/2004
	TUEV Sued, Dresden	10/2004
	STEAG Kraftwerk, Herne	10/2004, 12/2004
	University of Weimar	10/2004
	energeticals (e-concept), Munich	11/2004
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	Enertech EUT, Radebeul (company license)	11/2004
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	Technical University of Cottbus, Chair in Power Plant Engineering	12/2004
	Freudenberg Service, Weinheim	12/2004
2	003	
	Paper Factory, Utzenstorf, Switzerland	01/2003
	MAB Plant Engineering, Vienna, Austria	01/2003
	Wulff Energy Systems, Husum	01/2003
	Technip Benelux BV, Zoetermeer, Netherlands	01/2003
	ALSTOM Power, Baden, Switzerland	01/2003, 07/2003
	VER, Dresden	02/2003
	Rietschle Energieplaner, Winterthur, Switzerland	02/2003
	DLR, Leupholdhausen	04/2003

	Emden University of Applied Sciences, Department of Technology	05/2003
	Petterssson+Ahrends, Ober-Moerlen	05/2003
	SOFBID ,Zwingenberg (general EBSILON program license)	05/2003
	Ingenieurbuero Ostendorf, Gummersbach	05/2003
	TUEV Nord, Hamburg	06/2003
	Muenstermann GmbH, Telgte-Westbevern	06/2003
	University of Cali, Colombia	07/2003
	Atlas-Stord, Rodovre, Denmark	08/2003
	ENERKO, Aldenhoven	08/2003
	STEAG RKB, Leuna	08/2003
	eta Energieberatung, Pfaffenhofen	08/2003
	exergie, Dresden	09/2003
	AWTEC, Zurich, Switzerland	09/2003
	Energie, Timelkam, Austria	09/2003
	Electrowatt-EKONO, Zurich, Switzerland	09/2003
	LG, Annaberg-Buchholz	10/2003
	FZR Forschungszentrum, Rossendorf/Dresden	10/2003
	EnviCon & Plant Engineering, Nuremberg	11/2003
	Visteon, Kerpen	11/2003
	VEO Vulkan Energiewirtschaft Oderbruecke, Eisenhuettenstadt	11/2003
	Stadtwerke Hannover	11/2003
	SaarEnergie, Saarbruecken	11/2003
	Fraunhofer-Gesellschaft, Munich	12/2003
	Erfurt University of Applied Sciences, Department of Supply Engineering	12/2003
	SorTech, Freiburg	12/2003
	Mainova, Frankfurt	12/2003
	Energieversorgung Halle	12/2003
2002		
	Hamilton Medical AG, Rhaezuens, Switzerland	01/2002
	Bochum University of Applied Sciences, Department of Thermo- and Fluid Dynamics	01/2002
	SAAS, Possendorf/Dresden	02/2002
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DREWAG, Dresden		05/2002
SOFBID, Zwingenbe	erg	06/2002
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Dillinger Huette, Dilli	ngen	11/2002
G.U.N.T. Geraeteba (general license and	u, Barsbuettel training test benches)	12/2002
VEAG, Berlin (group	license)	12/2002
2001		
ALSTOM Power, Ba	den, Switzerland	01/2001, 06/2001 12/2001
KW2 B. V., Amersfo	ot, Netherlands	01/2001, 11/2001
Eco Design, Saitama	aken, Japan	01/2001
M&M Turbine Techn	ology, Bielefeld	01/2001, 09/2001
MVV Energie, Mann	heim	02/2001
Technical University Power Machinery ar	of Dresden, Department of and Plants	02/2001
PREUSSAG NOELL	., Wuerzburg	03/2001
Fichtner Consulting (company licenses a	•	04/2001
Muenstermann Gmb	H, Telgte-Westbevern	05/2001
SaarEnergie, Saarb	ruecken	05/2001

	Siemens, Karlsruhe (general license for the WinIS information system)	08/2001
	Neusiedler AG, Ulmerfeld, Austria	09/2001
	h s energieanlagen, Freising	09/2001
	Electrowatt-EKONO, Zurich, Switzerland	09/2001
	IPM Zittau/Goerlitz University of Applied Sciences (general license)	10/2001
	eta Energieberatung, Pfaffenhofen	11/2001
	ALSTOM Power Baden, Switzerland	12/2001
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	AG KKK - PGW Turbo, Leipzig	01/2000
	PREUSSAG NOELL, Wuerzburg	01/2000
	M&M Turbine Technology, Bielefeld	01/2000
	IBR Engineering Reis, Nittendorf-Undorf	02/2000
	GK, Hannover	03/2000
	KRUPP-UHDE, Dortmund (company license)	03/2000
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	SaarEnergie, Saarbruecken	05/2000, 08/2000
	DVO Data Processing Service, Oberhausen	05/2000
	RWTH Aachen University	06/2000
	VAUP Process Automation, Landau	08/2000
	Knuerr-Lommatec, Lommatzsch	09/2000
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	Compania Electrica, Bogota, Colombia	10/2000
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	Steinhaus Informationssysteme, Datteln (general license for process data software)	12/2000
19	99	
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Regensburg University of Applied Sciences	04/1999
Fichtner Consulting & IT, Stuttgart (company licenses and distribution)	07/1999
Technical University of Cottbus, Chair in Power Plant Engineering	07/1999
Technical University of Graz, Department of Thermal Engineering, Austria	11/1999
Ostendorf Engineering, Gummersbach	12/1999
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Technical University of Cottbus, Chair in Power Plant Engineering	05/1998
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