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COMPUTER SUBROUTINES FOR THE CALCULATION OF THERMO-PHYSICAL PROPERTIES OF WORKING FLUIDS USED IN ENERGY ENGINEERING

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#### INTRODUCTION

The application of electronic computers also in the field of energetics requires increasingly corresponding software for computer-aided design and optimization as well as automated operating of plants. According to these tendencies, scientific work for the mechanical placing at dispasal of substance data for all thermodynamic and thermohydraulic modellings of precesses had been started at the beginning of the seventhies.

This paper represents the working situation of 1985 as a summary and shows some selected scientific results.

SYMBOLS, INDEXES AND ABBREVIATIONS

nomenclature with dimension   dimensionless		sense		
n		material parameter		
P	l n	pressure		
1	temperature			
V	X specific valume			
s	G	specific entropy		
h	E	specific enthalpy		
u	*	specific internal energy		
×	10	dryness fraction specific heat		
C	φ	capacity		
a <sub>s</sub>		isentropic sonic speed		
η		dynamic viscosity		
λ		thermal conductivity		
G⁴		surface tension		
index		sense		
k		critical state		
t		triple state		
d		saturated state		
		saturated liquid		
11		dry saturated vapour		
SP		SUBPROGRAMM		
PS		programme set		

ASPECTS OF MODERN PLACING AT DISPOSAL OF SUBSTANCE DATA

Statements following are focussed on the problems of energetics and by that on the mostly used working fluids (pure substances).

New problems in preparing and making available thermophysical substance data have come out by microelec-

tronics and the fast availability of all-size computers connected by terminals and long-distance data transmission plants:

- complex placing at disposal of substance data by medium and large-size computers;
- simplified calculation of substance data by small-size and microcomputers and microprocessors respectively as well as developing of processes for the automated generation of such algorithmus (also for unsteady modellings by medium and large-size computers;
- establishment of data banks and attached dialog programmes for substance data by all-size computers;
- generation of equilibrium diagrammes on displays and plotters as working means;
- generation of printable vapour charts.

Fig. 1 shows how to realize these tasks at the Thermodynamics Department.

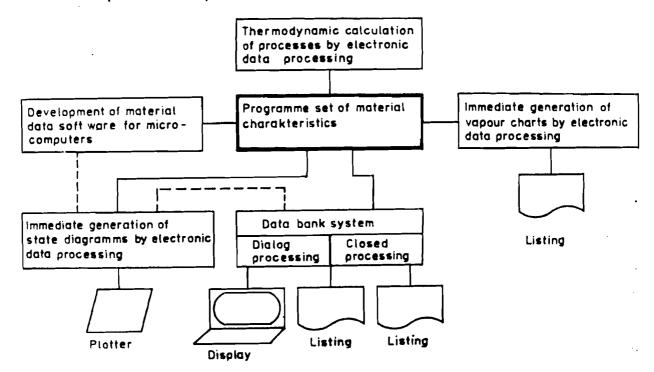


Fig. 1 Illustration of research objectives at the Thermodynamics Department

First of all, the central programme set for placing at disposal of substance data had been designed for calculating substance data for thermodynamic process calculations by large-size computers (1,2,3). The other working directions arranged radially in fig. 1 have been started later on. They use computable information by the programme set.

A SUBSTANCE DATA PROGRAMME SET FOR MEDIUM AND LARGE+SIZE COMPUTERS

As it is known, the quality of thermodynamic process calculations depend decisively upon substance data available. The concept of the programme system for comprehensive substance data computation is determined by:

- placing at disposal of substance data for the most inportant working fluids of energetics:
- computation of many thermophysical properties and their derivatives:
- realization of implicate thermodynamic functions with any pairs of the given quantities o.T.v.s.h.u by substance-independent calculations:
- aquisition of the laggest-possible range of state and fluid one and two-phase regions;
- selection of several equations of state (formulation) of different complexity and precision for the most important substances:
- guarantee of thermodynamic consistency between functions and especially at interphases.

WORKING FLUIDS

At present, working fluids as shown in fig 2 may be computed.

substance	equation of state	material parameter	
water	IAPS 1984 IFC 1968 IFC 1967	<b>8</b> 9	
}	IFC 1967 (techn.region) RIVKIN and	4	
	KREMENEVSKAJA /4/ VDI 1963	11 10	
ammonia	MARTIN - HOU - equation	20	
R11	(ILKA-calculation catalogue)	21	
R 12 R 13	151	22 23	
R 22 R 13 B1		24 25	
R 113 R 114		26 27	
R 502		28	
R 12	BAEHR and HICKEN	3	
carbondioxide	ALTUNIN, IUPAC resp.	5	
helium	ZEDERBERG	6	
sodium	PEE 161	7	
nitragen	unifled state equation	12	
helium	171	13	
oxig <b>e</b> n air	1	14 15	
methane	}	16	
ethane		17	
ethylene	<u> </u>	18	
15 substances	model of the semi ideal gas	1	

Fig. 2 Working fluids contained in the programme set of the Thermodynamics Department at Dresden University of Technology (1985)

According to manifold application, five formulations have been considered for water as the mostly used working fluid at energetics. Experiences with different equations from the point of view of thermodynamic process calculation shows /8/. Furthermore, some refrigerants and especially cooling fluids for nuclear reactors and gases for combustion computation are available.

## **FUNCTIONS**

The wide range of thermodynamic functions of state, transport quantities and derivatives (see fig. 3) of the programme set results from requirements of different process computations at energetics. Especially inverse functions for any given pairs of quantities p.T.v.s.h,u are placed at disposal. The dryness fraction x contained in relations indicates the functional capability of subprogrammes at fluid one and two-phase regions. The substance data programme set may be used in the shape of subprogrammes for each function shown in chart 1. Through a characteristic number, the desired substance and equation of state respectively may be

 $\eta = \eta (p,T,v,x)$  $p_s = p_s(T_s)$ choosen.  $\lambda = \lambda (p,T,v^*,x)$  $T_s = T_s (p_s)$ σ = σ (T) v = v(p,T,x)p, x = p, x (T, v) $c_p = c_p(p,T,v,x)$ T, x = T, x(p,v) $a_s = a_s(p,T,v^*,x)$  $s = s(p,T,v^*x)$  $\left(\frac{\partial p}{\partial T}\right) = \left(\frac{\partial p}{\partial T}\right)(p,T,v^*,x)$ h = h(p,T,v\*x)p,v,x=p,v,x(T,s) $\left(\frac{\partial V}{\partial T}\right)_{0} = \left(\frac{\partial V}{\partial T}\right)_{0} (p, T, V^{*}_{1} \times )$ p,v,x=p,v,x(T,h) $T_{v,x} = T_{v,x}(p,s)$  $\left(\frac{\partial p}{\partial v}\right) = \left(\frac{\partial p}{\partial p}\right) (p, T, v^*, x)$ T,v,x=T,v,x(p,h)p,T,x=p,T,x(v,s) $\left(\frac{\partial s}{\partial T}\right) = \left(\frac{\partial s}{\partial T}\right) (p, T, \vee^*, \times)$ p,T,x=p,T,x(s,h)p,T,x = p,T,x(v,u)\* - There is no necessity of the input of v as a given p,T,v,x=p,T,v,x(s,h)quantity

Fig. 3 Relations for thermodynamic quantities in the substance data programme set (1985)

### CALCULATION

All thermodynamic functions and derivatives are calculated substance-independently by means of iteration and numerical differentiation in subprogrammes of plane III. To do so, it is departed from substance-specific equations of state in reduced shape  $(v,S,h=f(\rho,T))$  at engineering formulation and  $\rho,s,h=f(T,v)$  at physical formulation as well as the vapour pressure function  $P_d=P_d(T_d)$  and their derivatives (see fig. 4, plane 3). This line of action has proved a success because of the possibility for controlling the thermodynamic consistency of calculated functions between each other and especially at interphases.

As an example, fig. 5 shows the internal calculation of the SP TVPSRE for functions p, T, X = f(p,s).

Departing from the pressure given, the attached limit cycle entropies are calculated and compared to the attached entropy in the phase test at first. After that, the actual calculations take place in the one and two-phase region. To avoid ineffective and confound iterations, algorithms have been written separately for engineering and physical formulations of equations of state (Those interesested will find detailed description in /10/).

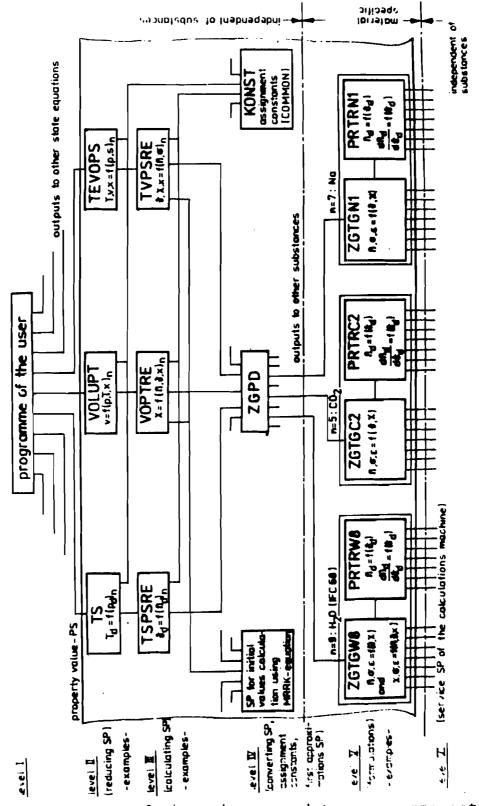
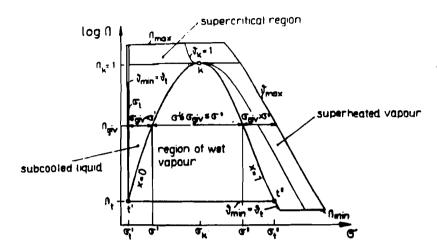


Fig. 4 Part of the substance data programme set.



physical formulation  $[\Pi, \sigma, \varepsilon = \Pi, \sigma, \varepsilon(\vartheta, \chi)]$ 

technical formulation  $[X, \sigma, \varepsilon = X, \sigma, \varepsilon (\Omega, \vartheta, x)]$ 

## Test of phases

- one-dimensional iteration of X<sup>t</sup> and  $X^*$  out of  $\Omega = \Omega(\mathfrak{V}_{S_1}X)$ , compensation to N<sub>giv</sub>
- 5'=5'(\$<sub>it</sub>,\t') σ"="σ"(δ;, χ")

## One phase region

- two-dimensional iteration of  $\Phi_{i*}$ compensation to  $G_{giv}$  is  $G = G(\frac{1}{2}, \frac{1}{2})$ , compensation to  $G_{giv}$
- one-dimensional iteration of  $\vartheta_{it}$  out of  $\sigma = \sigma(\Pi_{giv},\vartheta)$ , compensation to Ggiv • X<sub>it</sub>= X (Ngive Bit )

• 0', 0"= 0', 0"( | nov , 0s)

## Two phase region

$$\vartheta_{it} = \vartheta_s \left( \Pi_{giv} \right) \quad \times_{H^2} \frac{\sigma_{giv} - \sigma^t}{\sigma^* - \sigma^t} \quad \times_{H^2} \times + \times_{it} \left\{ x^s - x^t \right\}$$
with

- X', X and G', G' out of the test of phases
- 5', 5" out of the test of phases • X', X" = X', X" (nov. 3);

Fig. 5 Illustration of test of phases and iterative calculation at the example T,v,x=f(p,s)

## POSITE VALUE ITERATION EQUATIONS

All functions of which variables do not correspond to given quantities of stored equations of state are calcumbated iteratively. Hence, the question for the underlying prime values raises. The effectiveness of calculation depends decisively on the precision of prime values. For all the functional relations, shown in fig. 6, substance—independent equations have been placed at disposal in /11/ and /13/. Approximations are based on a particularly modified

Thermodynamic functions of state	Iterate initial equations needed							
	One phase region		Wet vapour region		Test of phases			
	PF	TF	PF	TF	PF	TF		
$T_s = T_s(\rho_s)$			$\vartheta_{\mathbf{g}} = \vartheta_{\mathbf{g}}(\Omega_{\mathbf{g}})$	3, - 3, (n, )	_	_		
v = v(p,T,x)	$\chi = \chi(\Omega, \vartheta)$		$\chi' = \chi'(\Omega_a, \vartheta_a)$ $\chi'' = \chi''(\Omega_a, \vartheta_a)$	1				
p,x = p,x(T,v)		$n = n(\vartheta, x)$						
$T_{x} = T_{x}(p_{y})$	$\vartheta = \vartheta(n, x)$	3 - 3(n,x)	<u> </u>	<del></del>	<u> </u>			
p,v,x = p,v,x (T,s)	$\chi = \chi(\vartheta,\sigma)$	N = N(3,5)						
$p_1v_1x = p_1v_1x (T,h)$	$\chi = \chi(\vartheta,\varepsilon)$	n = n(a,c)						
p,T,x=p,T,x (v,s)	ग्रे = ग्रे(४,७)	0 = 0(x, a)		$\hat{y}_g = \hat{y}_g(\chi,\sigma)$	$ \vartheta_a = \vartheta_a (X^i)  \vartheta_a = \vartheta_a (X^a) $	$\hat{y}^{\bullet} = \hat{y}^{\bullet}(X_{i})$ $\hat{y}^{\bullet} = \hat{y}^{\bullet}(X_{i})$		
$p_iT_ix = p_iT_ix (v_ih)$	<b>ϑ = ϑ(</b> 1,ε)		$ \begin{aligned} \vartheta_0 &= \vartheta_0 \left( \Upsilon, \varepsilon \right) \\ \chi'' &= \chi'' \left( \Upsilon, \varepsilon \right) \end{aligned} $		$\vartheta_* = \vartheta_*(\chi^*)$ $\vartheta_* = \vartheta_*(\chi^*)$	8 = 8 (Y')		
T, v, x = T, v, x (p, s)	$x = x(0,\alpha)$	<b>v -</b> v(n,0)						
T, v,x = T, v,x (p,h)	$ \begin{array}{c} \vartheta = \vartheta(0, \mathcal{E}) \\ \chi = \chi(0, \mathcal{E}) \end{array} $	ð <b>-</b> ð(ñ,£)			<del></del>			
$p_iT_iv_ix = p_iT_iv_ix(s_ih)$		$\theta = \vartheta(\sigma, \varepsilon)$ $\Omega = \Omega(\sigma, \varepsilon)$		· •	$\chi_i = \chi_i(\alpha_i)$ $\chi_i = \eta^{\alpha}(\alpha_i)$	$\hat{\sigma}_{\mathbf{s}} = \hat{\sigma}_{\mathbf{s}} \left( \sigma^{*} \right)$		
					$\hat{\mathcal{X}}_3 = \hat{\mathcal{X}}_3 (\sigma^a)$ $\hat{\mathcal{X}}^a = \hat{\mathcal{X}}^a (\sigma^a)$	ರಿ₃= ರಿ₃ (ರ*		

$$\begin{split} \Pi &= \frac{p}{p_k} \quad \vartheta = \frac{T}{T_k} \quad \chi = \frac{v}{v_k} \quad \begin{array}{c} \text{PF-physical} \\ \text{TF-technical} \end{array} \quad \text{formulation} \\ G' &= \frac{s \cdot T_k}{p_k \cdot v_k} \quad \mathcal{E} = \frac{h}{p_k \cdot v_k} \quad \text{s - saturation curve} \\ \quad \text{' - boiling curve} \quad \text{" - dew curve} \\ \end{split}$$

Fig. 6 Prime value iteration equations

Redlich-Kwong equation and linear setups for the vapour-pressure relation in the log  $p_d$  : 1, $T_d$ -plane. They are transmissible to other substances without the use of chart data and regression.

USE OF THE SUBSTANCE DATA PROGRAMME SET

At present, the use of the programme set for modellings and optimizations of power plant processes is in
the first place. The storage location needed depends upon
substance data functions called-in as well as substances
to be calculated:

properties out of the function of p and T: 14 % Byte inverse functions: 60 % Byte derivatives: 5 % Byte

working fluids depending on the complexity of the equation of state:

2...15 % Syte

The computation time needed for one characteristic point is also determined by the complexity of the choosen equation of state. Some selected examples might be noted (TOPP DESE 6):

properties as a function of p and 7: (.302...3.08 s inverse functions: 0.08 ...0.2 s

For the direct and daily use, a dialog inquiry programme is available (storage location of 20 % Dyte).

GENERATION OF THERMODYNAMIC EQUILIBRIUM DIAGRAMMES

Decause of the accomplishment of many logical and computation processes by fast available computers, visual working means as outline and test diagrammes for thermodynamic calculations have an increasing significance. It has come out a necessary task to generate them with the most different state persmeters and also in coordinates unusual up to now on plotters and graphical screens.

Departing from many programmos being already in

existence for thermophysical state parameters, a programme system for medium and large-size computers has been developed with using the substance data programme set at Thermodynamics Department of the Dresden University of Technology. The possibilities are as follows:

- representation of any quantities in any coordinates with different axis graduations in closed curves;
- substance-independent diagram computation and selective representation of several substances and equations of state respectively in one diagram for the purpose of comparison;
- drawing of any cut-outs and enlargements inclusive one and two-phase regions;
- interpolation of all coordinate values only out of supporting values to be computed

in the one-phase region in the frame of temperature and pressure (isothermal),

in the two-phase region in the frame of temperature and dryness fraction (isothermal);

- production of diagrams for the purpose of comparison as well as reading off with high precision.

Fig. 7 illustrates the principle of diagramm generation.

A detailed description of algorithms contains /9/.

Fig. 8 represents a photo copy of a h s-diagram of water according to IFC '68 drawn by the DIGIGRAF-plotter / 12 / as part of steam turbine calculation (original size 100 cm x 80 cm, ball-point pen drawing).

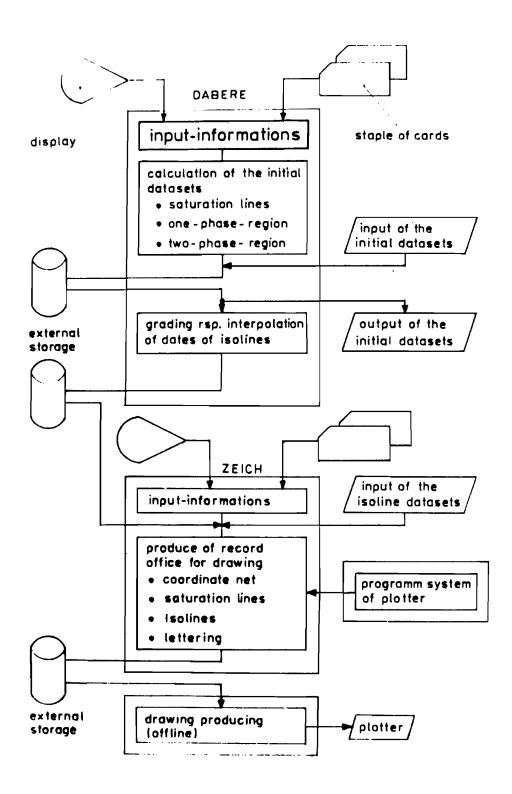


Fig. 7 Principle of computing and automated drawing of equilibrium diagrams

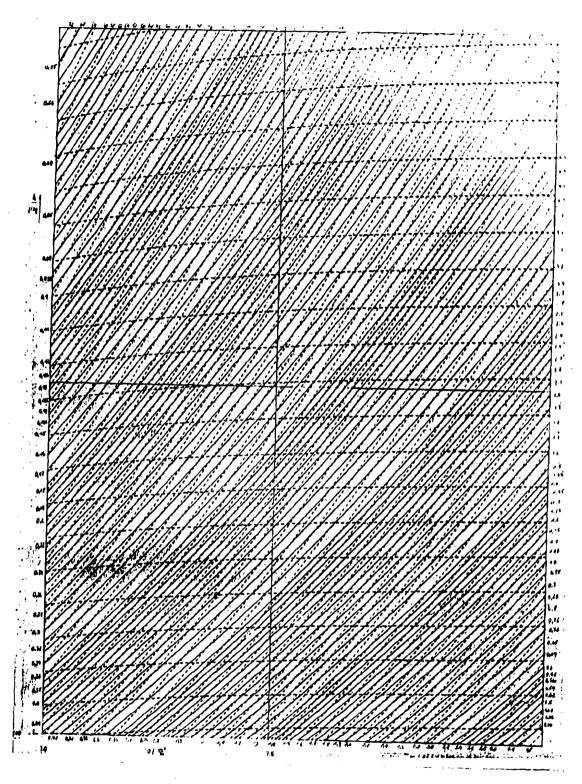


Fig. 8 Part of a  $h_1$  s-diagram; region of superheated steam.

# GENPLIFIED SUBSTANCE DATA COMPUTATION ON DICROCOMPUTERS

The use of personnel computers at design departments and microprocessors for operating energy plants requires software for simplified modellings of basic units and processes in a large scale. Because of limited resources of microcomputers, an effective placing at disposal of substance data is required with respect to demands of calculation time and storage location. Especially the small extension of terms has to be considered. Desides elaborating suitable and simplified algorithms for microcomputers, research work is also done with respect to their automated generation on large-size computers by use of the substance data programme set. This work is focused on a programme system making available simplified algorithms for a given range of state at required precision and with quantitative consideration of the thermodynamic consistency.

Three traditional anthem of solution are possible to compute substance data by microcomputers. They are illustrated in fig. 9 and should be discussed shortly.

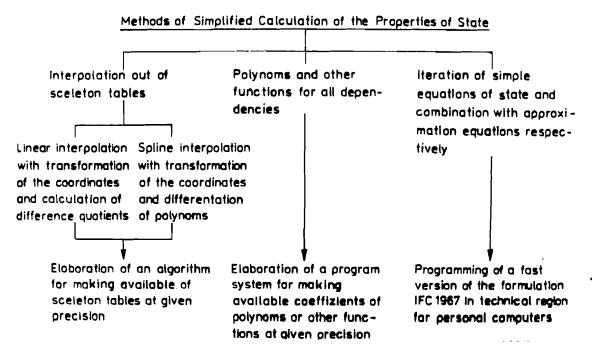


Fig. 9 Pathes of solution for simplified substance data computation by microcomputers

The number of supporting values ejected in the primary store limits the range of state computable by the first method of interpolation. Because of carrying out all calculations with the same supporting data, thermodynamic consistency between functions and at interphases is well guaranteed. On account of simple mathematical operations, the interpolation is very suitable to computers. Presuming the interpolation in the primary store, computation time needed for finding of one characteristic point becomes relatively short. A few supporting values will do for calculations when adapting the transformation of coordinates in connection with spline-interpolation to the true thermodynamic behavior.

When calculating functions of state by simple functions and polynome, the region of state covered is limited by the maximum degree of polynoms. It results from significant numbers needed for coefficients as well as the maximum number of coefficients for polynoms in the primary store. The quantitative consideration of the thermodynamic consistency between functions and at interphases forms a special problem within this path of solution. However, very little computation time is needed when using high-performance polynoms.

Referring to the third path, the computable region of state depends upon equations of state used. When determining implicite functions iteratively out of equations of state, consistency is controllable but computation time increases considerably. On the other hand, a combination of equations of state and polynoms or interpolations are favourable. The altogether long computation time and relatively high demands for storage location forbid the direct use at process calculations but they are well sufficient for substance data banks on personnel computers.

SUMMARY

The represented acientific work for processing and

making available of substance data deliver solutions for medium and large-size computers as well as microcomputers as follows:

- informations programmes for substance data;
- complex placing at disposal of substance data;
- generation of simplified substance date algorithms;
- generation of equilibrium diagrammes and printable vapour charts.

A central problem of present research work is given by the automated generation of simplified algorithms for aubstance data.

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